

① (i) plane

② Net magnetic flux through any closed surface is zero - $\sum B \cdot dS = 0$

③ (ii) q_1 and q_2 are +ve

④ (iii) $E_n = \frac{-13.6}{n^2} eV$

⑤ (i) and (iii)

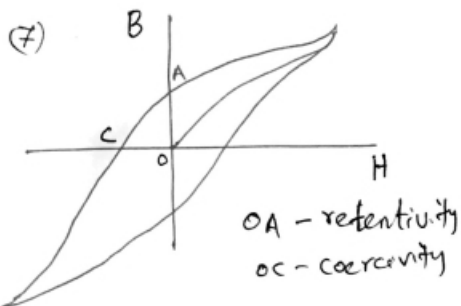
⑥ (a) $F = qvB$ since or $\vec{F} = q(\vec{v} \times \vec{B})$

⑥ $B = \frac{qF}{qv \sin \theta}$

$$= \frac{q}{v \sin \theta}$$

$$= \frac{q \times m}{s}$$

$$= \text{Ns/cm}$$



⑧ Anticlock wise.

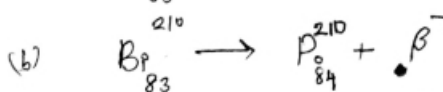
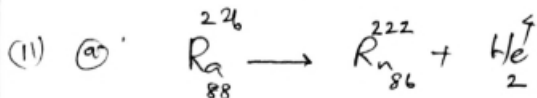
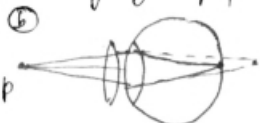
When the loop is moving towards the magnetic field, magnetic flux changes and induced current will flow accordingly to produce a field opposite to the present field.

⑨ (a) Eddy current

(b) Induction furnace

(iii) Induction braking

⑩ (a) Long sight / farsightedness



(12) (a) $C_s = \frac{C_1 C_2}{C_1 + C_2} = \frac{C \times 3C}{C + 3C} = \frac{3C}{4}$

$\left. \begin{array}{l} C_1 = C \\ C_2 = 3C \end{array} \right\} = 3C$

$$Q = CV$$

$$= \frac{3C}{4} \times 18$$

$$= \frac{27C}{2}$$

$$V_1 = \frac{Q}{C_1} = \frac{27C}{2 \times C} = \frac{27}{2} V = 13.5V$$

$$V_2 = \frac{Q}{C_2} = \frac{27C}{2 \times 3C} = \frac{9C}{2} = 4.5V$$

(13) (a) $V = \frac{1}{\sqrt{\mu \epsilon}}$

(b) (i) γ -ray - emitted by radio active nuclei

(ii) Visible - λ from 700-400nm

(iii) X-ray - Bombarding metal target by e^-

(iv) Microwave - Radar system

(14) (a) Dispersion



(b) Violet < Blue < Yellow

15) Lyman, Balmer, Paschen, Brackette, Pfund series

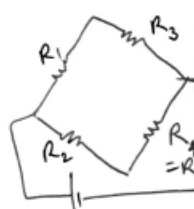
(b) $E = h\nu$ — (1)

$E = 2.3 \text{ eV}$
 $= 3.3 \times 1.6 \times 10^{-19} \text{ J}$

$\nu = \frac{E}{h}$
 $= \frac{3.3 \times 1.6 \times 10^{-19}}{6.6 \times 10^{-34}}$
 $= 0.8 \times 10^{15} \text{ Hz}$

(b) statement $\frac{dn}{dt} \propto N \frac{dn}{dt} = -\lambda n$
 Derivation of $n_t = n_0 e^{-\lambda t}$

(17) (a) $\frac{R_1 + R_3}{R_2} = \frac{R_3}{R_4}$
 $\frac{20}{40} = \frac{40}{R}$
 $R = 80 \Omega$



(b) $R_{\text{eff}} = (R_1 + R_3) \parallel (R_2 + R_4)$
 $R_{\text{eff}} = \frac{60 \times 120}{60 + 120} = 40 \Omega$
 $I = \frac{V}{R_{\text{eff}}} = \frac{20}{40} = 0.5 \text{ A}$

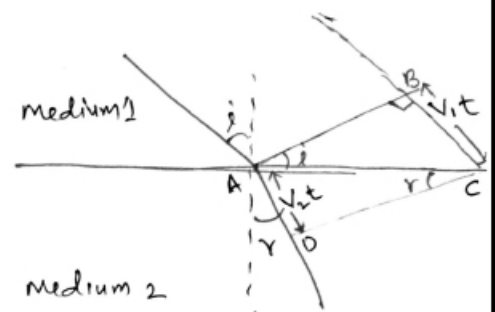
(18) (a) Nm^2/C OR Vm .

(b) Derivation of $E = \frac{1}{4\pi\epsilon_0} \frac{2\lambda}{r}$

(19) (a) Ampere circuital theorem.

(b) Derivation of $B = \mu_0 n I$

(20)



$\sin i = \frac{BC}{AC} = \frac{V_1 t}{AC}$ — (1)

$\sin r = \frac{AB}{AC} = \frac{V_2 t}{AC}$

$\frac{\sin i}{\sin r} = \frac{V_1}{V_2} = \text{Constant}$

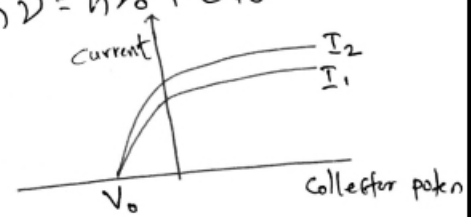
(21) ~~Work done = qV_0~~

(a) $h\nu = \phi_0 + K E_{\text{max}}$

(OR) $h\nu = h\nu_0 + K E_{\text{max}}$

(OR) $h\nu = h\nu_0 + eV_0$

(b)



(c) $\nu = 1.5 \nu_0$

when frequency reduced to half

$\nu = 0.5 \nu_0$ which means

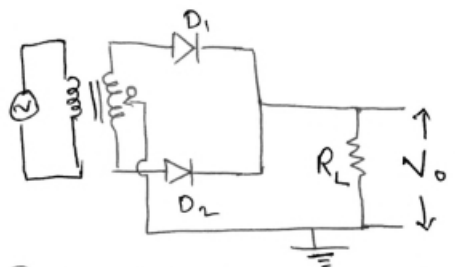
$\nu < \nu_0$

No photoelectric emission

$\therefore I' = 0$

(3)

(22)



Explanation of FW rectifier

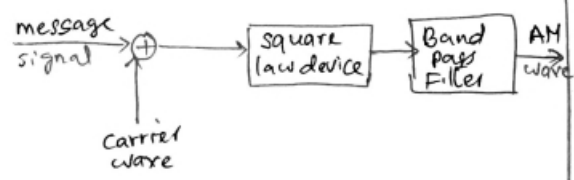
(23) (a) Amplitude of the carrier wave is varied in accordance with the instantaneous value of message signal.

(b)
$$\mu = \frac{A_m}{A_c}$$

$$= \frac{10}{20}$$

$$= \underline{\underline{0.5}}$$

(c)



(24) (a) Circuit diagram

$E \propto l$

$$\frac{E_1}{E_2} = \frac{l_1}{l_2}$$

(b) Internal resistance

$$r = R \frac{(l_1 - l_2)}{l_2}$$

$$= 9.5 \frac{(76.3 - 64.8)}{64.8}$$

$$= \frac{9.5 \times 11.5}{64.8} = \underline{\underline{1.686 \Omega}}$$

(25) (a) Tuning of radio

(b) Since the circuit is in resonance,

$$Z = R$$

$$X_L = X_C$$

$$\therefore I = \frac{V}{Z} = \frac{110}{48} = 2.29 \text{ A}$$

$$f_r = \frac{1}{2\pi\sqrt{LC}}$$

$$= \frac{1}{2 \times 3.14 \sqrt{0.38 \times 27 \times 10^{-6}}}$$

$$= \underline{\underline{49.7 \text{ Hz}}}$$

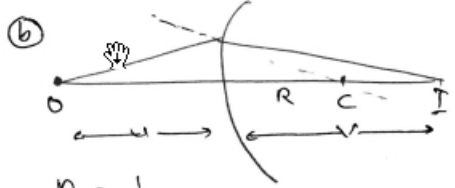
(c) Capacity changes (increases)

$$X_L \neq X_C$$

$$Z > R$$

Current decreases.

(26) (a) Derivation of $\frac{n_2}{v} - \frac{n_1}{u} = \frac{n_2 - n_1}{R}$



(b)

$$n_1 = 1$$

$$n_2 = 1.5$$

$$v = +100 \text{ cm}$$

$$R = +20 \text{ cm}$$

$$\frac{n_2}{v} - \frac{n_1}{u} = \frac{n_2 - n_1}{R}$$

$$\frac{1.5}{100} - \frac{1}{u} = \frac{0.5}{20}$$

$$\frac{1}{u} = \frac{1.5}{100} - \frac{5}{200} \Rightarrow u = \underline{\underline{-100 \text{ cm}}}$$