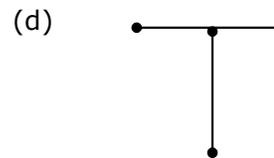
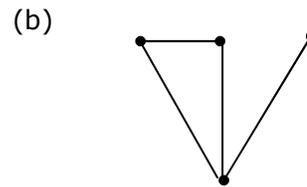
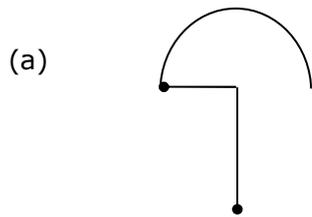
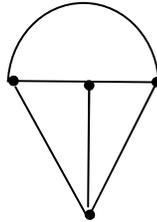
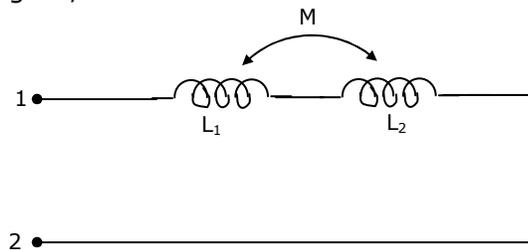


**Q.1 – Q.30 Carry One Mark Each**

1. Consider the network graph shown in figure. Which one of the following is NOT a 'tree' of this graph?



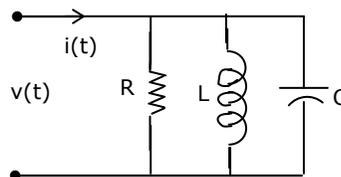
2. The equivalent inductance measured between the terminals 1 and 2 for the circuit shown in figure, is



- (a)  $L_1 + L_2 + M$       (b)  $L_1 + L_2 - M$       (c)  $L_1 + L_2 + 2M$       (d)  $L_1 + L_2 - 2M$

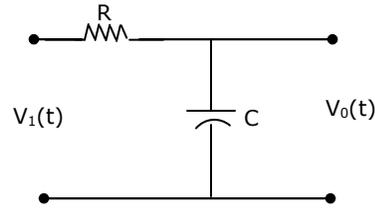
3. The circuit shown in Fig.Q.3, with  $R = \frac{1}{3} \Omega, L = \frac{1}{4} H, C = 3F$  has input voltage  $v(t) = \sin 2t$ . The resulting current  $i(t)$  is

- (a)  $5 \sin(2t + 53.1^\circ)$   
 (b)  $5 \sin(2t - 53.1^\circ)$   
 (c)  $25 \sin(2t + 53.1^\circ)$   
 (d)  $25 \sin(2t - 53.1^\circ)$

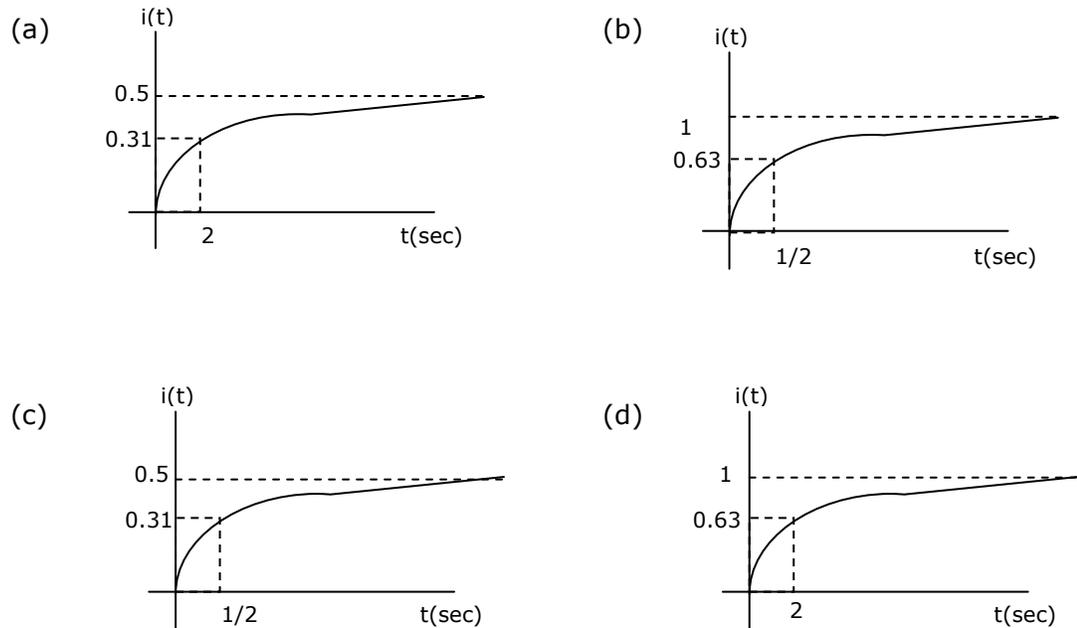
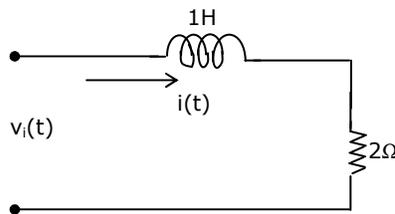


4. For the circuit shown in Fig.Q.4, the time constant  $RC = 1\text{ms}$ . The input voltage is  $v_i(t) = \sqrt{2} \sin 10^3 t$ . The output voltage  $v_o(t)$  is equal to

- (a)  $\sin(10^3 t - 45^\circ)$   
 (b)  $\sin(10^3 t + 45^\circ)$   
 (c)  $\sin(10^3 t - 53^\circ)$   
 (d)  $\sin(10^3 t + 53^\circ)$



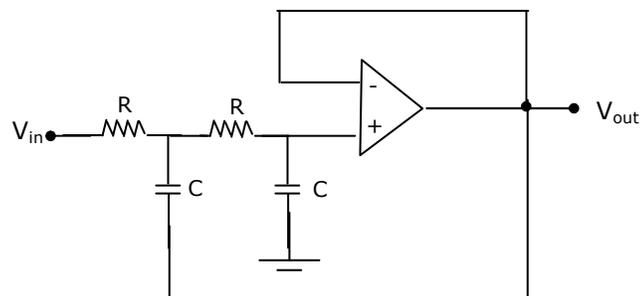
5. For the R-L circuit shown in Fig.Q.5, the input voltage  $v_i(t) = u(t)$ . The current  $i(t)$  is



6. The impurity commonly used for realizing the base region of a silicon n-p-n transistor is

- (a) Gallium                      (b) Indium                      (c) Boron                      (d) Phosphorus

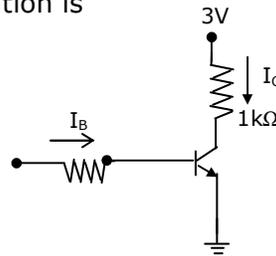
7. If for a silicon n-p-n transistor, the base-to-emitter voltage ( $V_{BE}$ ) is 0.7V and the collector-to-base voltage ( $V_{CB}$ ) is 0.2V, then the transistor is operating in the  
(a) normal active mode (b) saturation mode  
(c) inverse active mode (d) cutoff mode
8. Consider the following statements  $S_1$  and  $S_2$ .  
 $S_1$ : The  $\beta$  of a bipolar transistor reduces if the base width is increased.  
 $S_2$ : The  $\beta$  of a bipolar transistor increases if the doping concentration in the base is increased  
Which one of the following is correct?  
(a)  $S_1$  is FALSE and  $S_2$  is TRUE (b) both  $S_1$  and  $S_2$  are TRUE  
(c) both  $S_1$  and  $S_2$  are FALSE (d)  $S_1$  is TRUE and  $S_2$  is FALSE
9. An ideal op-amp is an ideal  
(a) voltage controlled current source (b) voltage controlled voltage source  
(c) current controlled current source (d) current controlled voltage source
10. Voltage series feedback (also called series shunt feedback) results in  
(a) increase in both input and output impedances  
(b) decrease in both input and output impedances  
(c) increase in input impedance and decrease in output impedance  
(d) decrease in input impedance and increase in output impedance
11. The circuit in Figure is a



- (a) low-pass filter (b) high-pass filter  
(c) band-pass filter (d) band-reject filter

12. Assuming  $V_{Cesat}=0.2V$  and  $\beta = 50$ , the minimum base current ( $I_B$ ) required to drive the transistor in Fig.Q.12 to saturation is

- (a)  $56 \mu A$
- (b)  $140 mA$
- (c)  $60 \mu A$
- (d)  $3 mA$



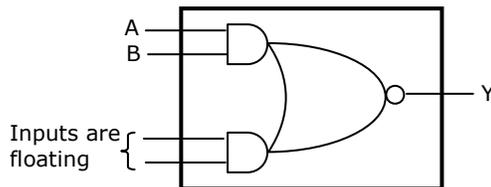
13. A master slave flip-flop has the characteristic that
- (a) change in the input immediately reflected in the output
  - (b) change in the output occurs when the state of the master is affected
  - (c) change in the output occurs when the state of the slave is affected
  - (d) both the master and the slave states are affected at the same time
14. The range of signed decimal numbers that can be represented by 6-bite 1's complement number is
- (a) -31 to +31
  - (b) -63 to +64
  - (c) -64 to +63
  - (d) -32 to +31
15. A digital system is required to amplify a binary-encoded audio signal. The user should be able to control the gain of the amplifier from a minimum to a maximum in 100 increments. The minimum number of bits required to encode, in straight binary is
- (a) 8
  - (b) 6
  - (c) 5
  - (d) 7
16. Choose the correct one from among the alternatives A,B,C,D after matching an item from Group 1 with the most appropriate item in Group 2.

| Group 1           | Group 2                               |
|-------------------|---------------------------------------|
| P. Shift register | 1. Frequency division                 |
| Q. Counter        | 2. Addressing in memory chips         |
| R. Decoder        | 3. Serial to parallel data conversion |

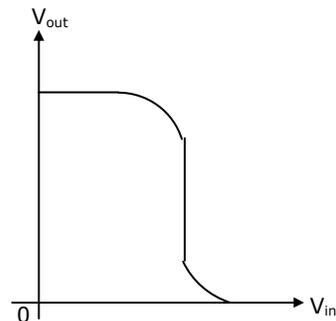
- (a) P – 3 Q – 2 R - 1
- (b) P – 3 Q – 1 R - 2
- (c) P – 2 Q – 1 R – 3
- (d) P – 1 Q – 2 R - 2

17. Figure shows the internal schematic of a TTL AND-OR-Invert (AOI) gate. For the inputs shown in Figure, the output Y is

- (a) 0
- (b) 1
- (c) AB
- (d)  $\overline{AB}$



18. Figure is the voltage transfer characteristic of
- (a) an NMOS inverter with enhancement mode transistor as load
  - (b) an NMOS inverter with depletion mode transistor as load
  - (c) A CMOS inverter
  - (d) A BJT inverter

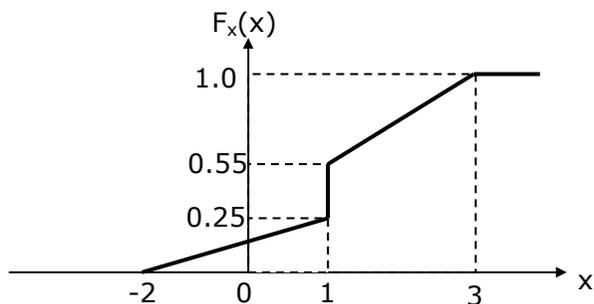


19. The impulse response  $h[n]$  of a linear time-invariant system is given by  $h[n] = u[n + 3] + u[n - 2] - 2u[n - 7]$

where  $u[n]$  is the unit step sequence. The above system is

- (a) stable but not causal
- (b) stable and causal
- (c) causal but unstable
- (d) unstable and not causal

20. The distribution function  $F_x(x)$  of a random variable X is shown in Fig.Q.20. the probability that  $X = 1$  is



- (a) zero
- (b) 0.25
- (c) 0.55
- (d) 0.30

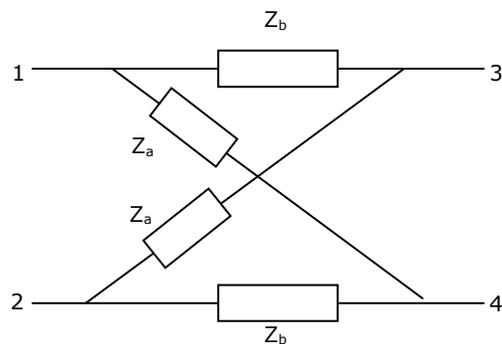
21. The z-transform of a system is  $H(z) = \frac{z}{z - 0.2}$   
If the ROC is  $|z| < 0.2$ , then the impulse response of the system is  
(a)  $(0.2)^n u[n]$  (b)  $(0.2)^n u[n - 1]$   
(c)  $-(0.2)^n u[n]$  (d)  $-(0.2)^n u[n - 1]$
22. The Fourier transform of a conjugate symmetric function is always  
(a) imaginary (b) conjugate anti-symmetric  
(c) real (d) conjugate symmetric
23. The gain margin for the system with open-loop transfer function  $G(s)H(z) = \frac{2(1+z)}{s^2}$ , is  
(a)  $\infty$  (b) 0 (c) 1 (d)  $-\infty$
24. Given the  $G(s)H(z) = \frac{K}{s(s+1)(s+3)}$ , the point of intersection of the asymptotes of the root loci with the real axis is  
(a) -4 (b) 1.33 (c) -1.33 (d) 4
25. In a PCM system, if the code word length is increased from 6 to 8 bits, the signal to quantization noise ratio improves by the factor  
(a)  $\frac{8}{6}$  (b) 12 (c) 16 (d) 8
26. An AM signal is detected using an envelope detector. The carrier frequency and modulating signal frequency are 1 MHz and 2 KHz respectively. An appropriate value for the time constant of the envelope detector is  
(a) 500  $\mu$ sec (b) 20  $\mu$ sec (c) 0.2  $\mu$ sec (d) 1  $\mu$ sec
27. An AM signal and a narrow-band FM signal with identical carriers, modulating signals and modulation indices of 0.1 are added together. The resultant signal can be closely approximated by  
(a) broadband FM (b) SSB with carrier  
(c) DSB-SC (d) SSB without carrier

28. In the output of a DM speech encoder, the consecutive pulses are of opposite polarity during time interval  $t_1 \leq t \leq t_2$ . This indicates that during this interval
- the input to the modulator is essentially constant
  - the modulator is going through slope overload
  - the accumulator is in saturation
  - the speech signal is being sampled at the Nyquist rate
29. The phase velocity of an electromagnetic wave propagating in a hollow metallic rectangular waveguide in the  $TE_{10}$  mode is
- equal to its group velocity
  - less than the velocity of light in free space
  - equal to the velocity of light in free space
  - greater than the velocity of light in free space
30. Consider a lossless antenna with a directive gain of +6db. If 1mW of power is fed to it the total power radiated by the antenna will be
- 4mW
  - 1mW
  - 7mW
  - $\frac{1}{4}$  mW

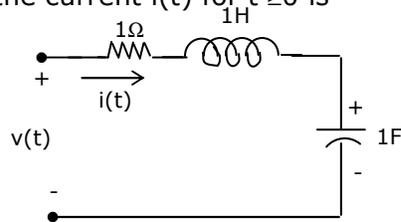
**Q.31 – Q.90 Carry Two Marks Each**

31. For the lattice circuit shown in Fig. Q.31,  $Z_a = j2\Omega$  and  $Z_b = 2\Omega$ . The values of the open circuit impedance parameters  $Z = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}$  are

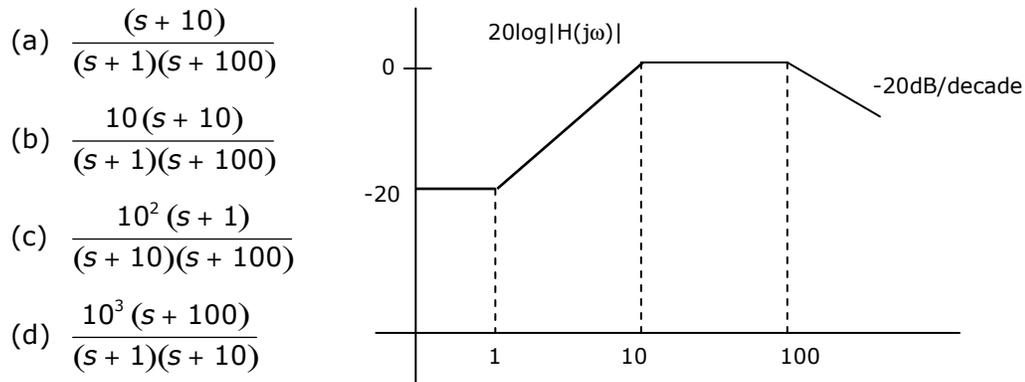
- $\begin{bmatrix} 1 - j & 1 + j \\ 1 + j & 1 + j \end{bmatrix}$
- $\begin{bmatrix} 1 - j & 1 + j \\ 1 + j & 1 - j \end{bmatrix}$
- $\begin{bmatrix} 1 + j & 1 + j \\ 1 - j & 1 - j \end{bmatrix}$
- $\begin{bmatrix} 1 + j & -1 + j \\ 1 - j & 1 - j \end{bmatrix}$



32. The circuit shown in Fig.Q.32 has initial current  $i_L(0^-) = 1A$  through the inductor and an initial voltage  $V_c(0^-) = -1V$  across the capacitor. For input  $v(t) = u(t)$ , the Laplace transform of the current  $i(t)$  for  $t \geq 0$  is



- (a)  $\frac{s}{s^2 + s + 1}$       (b)  $\frac{s + 2}{s^2 + s + 1}$       (c)  $\frac{s - 2}{s^2 + s + 1}$       (d)  $\frac{s - 2}{s^2 + s - 1}$
33. Consider the Bode magnitude plot shown in Fig.33. The transfer function  $H(s)$  is



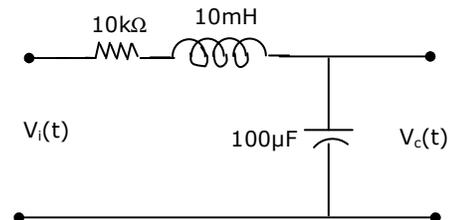
- (a)  $\frac{(s + 10)}{(s + 1)(s + 100)}$   
 (b)  $\frac{10(s + 10)}{(s + 1)(s + 100)}$   
 (c)  $\frac{10^2(s + 1)}{(s + 10)(s + 100)}$   
 (d)  $\frac{10^3(s + 100)}{(s + 1)(s + 10)}$
34. The transfer function  $H(s) = \frac{V_o(s)}{V_i(s)}$  of an R-L-C circuit is given by

$$H(s) = \frac{10^6}{s^2 + 20s + 10^6}$$

the Quality factor (Q-factor) of this circuit is

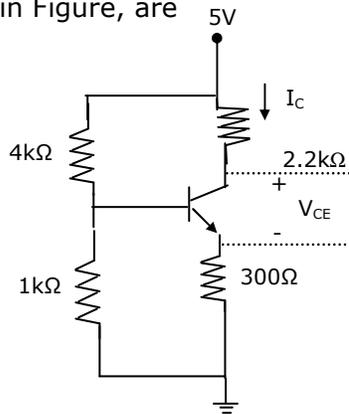
- (a) 25      (b) 50      (c) 100      (d) 5000
35. For the circuit shown in Fig.Q.35, the initial conditions are zero. Its transfer function  $H(s) = \frac{V_c(s)}{V_i(s)}$  is

- (a)  $\frac{1}{s^2 + 10^6s + 10^6}$       (b)  $\frac{10^6}{s^2 + 10^3s + 10^6}$   
 (c)  $\frac{10^3}{s^2 + 10^3s + 10^6}$       (d)  $\frac{10^6}{s^2 + 10^6s + 10^6}$





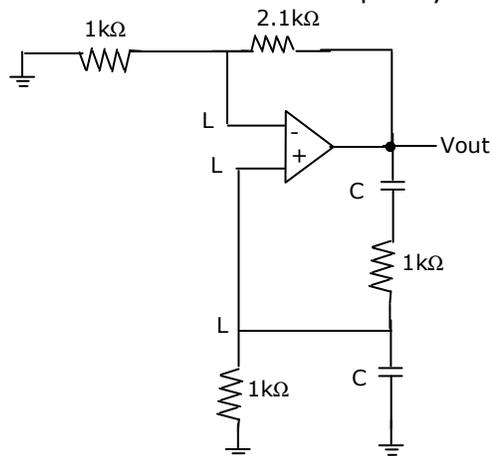
42. The drain of an n-channel MOSFET is shorted to the gate so that  $V_{GS} = V_{DS}$ . The threshold voltage ( $V_T$ ) of MOSFET is 1V. If the drain current ( $I_D$ ) is 1 mA for  $V_{GS} = 2V$ , then for  $V_{GS} = 3V$ ,  $I_D$  is  
 (a) 2 mA (b) 3 mA (c) 9 mA (d) 4 mA
43. The longest wavelength that can be absorbed by silicon, which has the bandgap of 1.12eV, is  $1.1\mu\text{m}$ . If the longest wavelength that can be absorbed by another material is  $0.87\mu\text{m}$ , then the bandgap of this material is  
 (a) 1.416 eV (b) 0.886 eV (c) 0.854 eV (d) 0.706 eV
44. The neutral base width of a bipolar transistor, biased in the active region, is  $0.5\mu\text{m}$ . the maximum electron concentration and the diffusion constant in the base are  $10^{14}/\text{cm}^3$  and  $D_n = 25\text{ cm}^2/\text{sec}$  respectively. Assuming negligible recombination I the base, the collector current density is (the electron charge is  $1.6 \times 10^{-19}$  coulomb)  
 (a)  $800\text{ A}/\text{cm}^2$  (b)  $8\text{ A}/\text{cm}^2$  (c)  $200\text{ A}/\text{cm}^2$  (d)  $2\text{ A}/\text{cm}^2$
45. Assuming that the  $\beta$  of the transistor is extremely large and  $V_{BE} = 0.7V$ ,  $I_C$  and  $V_{CE}$  in the circuit shown in Figure, are



- (a)  $I_C = 1\text{mA}, V_{CE} = 4.7V$  (b)  $I_C = 0.5\text{mA}, V_{CE} = 3.75V$   
 (c)  $I_C = 1\text{mA}, V_{CE} = 2.5V$  (d)  $I_C = 0.5\text{mA}, V_{CE} = 3.9V$
46. A bipolar transistor is operating in the active region with a collector current of 1mA. Assuming that the  $\beta$  of the transistor is 100 and the thermal voltage ( $V_T$ ) is 25 mV, the transconductance ( $g_m$ ) and the input resistance ( $r_\pi$ ) of the transistor in the common emitter configuration, are  
 (a)  $g_m = 25\text{mA}/V$  and  $r_p = 15.625\text{k}\Omega$  (b)  $g_m = 40\text{mA}/V$  and  $r_p = 4.0\text{k}\Omega$   
 (c)  $g_m = 25\text{mA}/V$  and  $r_p = 2.5\text{k}\Omega$  (d)  $g_m = 40\text{mA}/V$  and  $r_p = 2.5\text{k}\Omega$

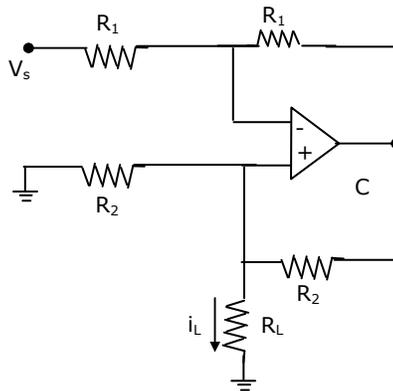
47. The value of C required for sinusoidal oscillations of frequency 1kHz in the circuit of Fig.Q.47 is

- (a)  $\frac{1}{2p} mF$   
 (b)  $2p mF$   
 (c)  $\frac{1}{2p\sqrt{6}} mF$   
 (d)  $2p\sqrt{6} mF$



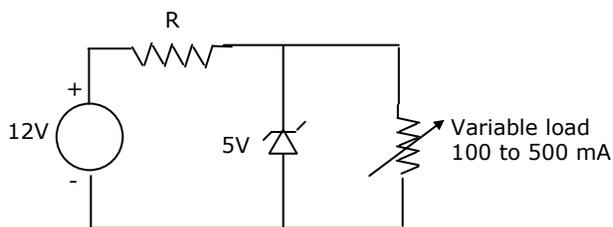
48. In the op-amp circuit given in Fig.Q.48, the load current  $I_L$  is

- (a)  $-\frac{n_s}{R_2}$   
 (b)  $\frac{n_s}{R_2}$   
 (c)  $-\frac{n_s}{R_L}$   
 (d)  $\frac{n_s}{R_L}$



49. In the voltage regulator shown in Fig.Q.49, the load current can vary from 100mA to 500mA. Assuming that the Zener diode is ideal (i.e., the Zener knee current is negligibly small and Zener resistance is zero in the breakdown region), the value of R is

- (a)  $7\Omega$   
 (b)  $70\Omega$   
 (c)  $\frac{70}{3} \Omega$   
 (d)  $14\Omega$

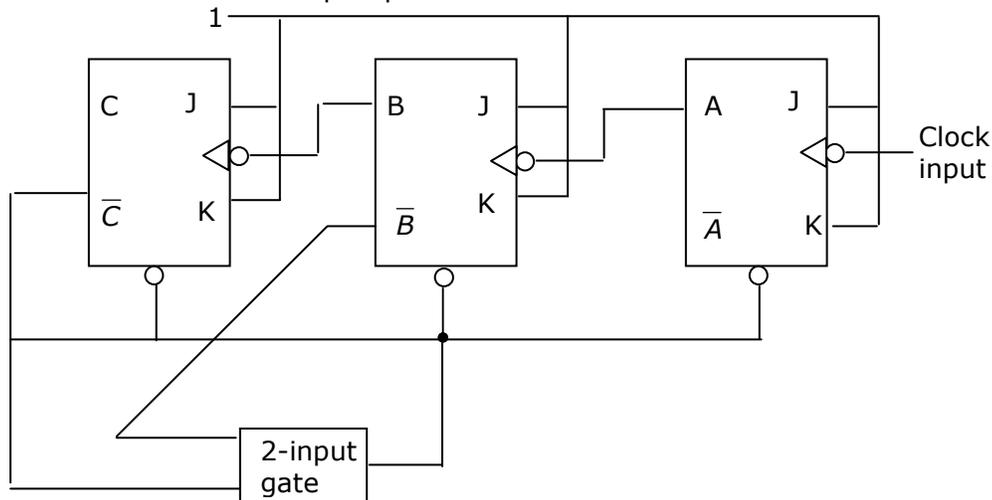


50. In a full-wave rectifier using two ideal diodes,  $V_{dc}$  and  $V_m$  are the dc and peak values of the voltage respectively across a resistive load. If PIV is the peak inverse voltage of the diode, then the appropriate relationships for this rectifier are

- (a)  $V_{dc} = \frac{V_m}{p}, PIV = 2V_m$                       (b)  $V_{dc} = 2 \frac{V_m}{p}, PIV = 2V_m$



56. In the modulo-6 ripple counter shown in Figure, the output of the 2-input gate is used to clear the J-K flip-flops.



- The 2-input gate is:  
 (a) a NAND gate      (b) a NOR gate      (c) an OR gate      (d) an AND gate
57. Consider the sequence of 8085 instructions given below.  
 LXI H, 9258      MOV A, M,      CMA,      MOV M, A  
 Which one of the following is performed by this sequence?  
 (a) contents of location 9258 are moved to the accumulator  
 (b) contents of location 9258 are compared with the contents of the accumulator  
 (c) contents of location 8529 are complemented and stored in location 8529  
 (d) contents of location 5892 are complemented and stored in location 5892
58. A Boolean function  $f$  of two variables  $x$  and  $y$  is defined as follows:  
 $f(0,0) = f(0,1) = f(1,1) = 1; f(1,0) = 0$   
 Assuming complements of  $x$  and  $y$  are not available, a minimum cost solution for realizing  $f$  using only 2-input NOR gates and 2-input OR gates (each having unit cost) would have a total cost of  
 (a) 1 unit      (b) 4 unit      (c) 3 unit      (d) 2 unit
59. It is desired to multiply the numbers 0AH by 0BH and store the result in the accumulator. The numbers are available in registers B and C respectively. A part of the 8085 program for this purpose is given below:  
 MVI A, 00H  
 Loop; - - - - -

.....  
HLT END

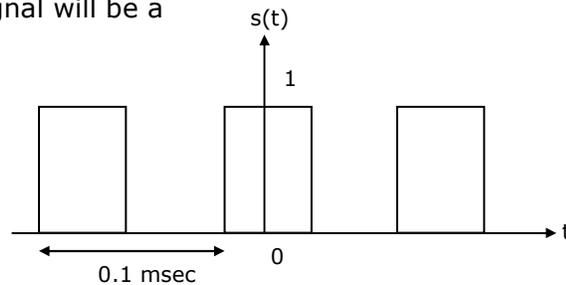
The sequence of instruction to the complete the program would be

- (a) JNZ LOOP, ADD B, DCR C
- (b) ADD B, JNZ LOOP, DCR C
- (c) DCR C, JNZ LOOP, ADD B
- (d) ADD B, DCR C, JNZ LOOP

60. A 1 kHz sinusoidal signal is ideally sampled at 1500 samples/sec and the sampled signal is passed through an ideal low-pass filter with cut-off frequency 800 Hz. The output signal has the frequency
- (a) zero Hz
  - (b) 0.75 kHz
  - (c) 0.5 kHz
  - (d) 0.25 kHz

61. A rectangular pulse train  $s(t)$  as shown in Fig.Q.61 is convolved with the signal  $\cos^2(4\pi \cdot 10^3 t)$ . the convolved signal will be a

- (a) DC
- (b) 12 kHz sinusoid
- (c) 8 kHz sinusoid
- (d) 14 kHz sinusoid



62. Consider the sequence  $x[n] = \begin{bmatrix} 4 - j5 & 1 + j2 & 4 \\ 4 & 1 & 4 \end{bmatrix}$

The conjugate anti-symmetric part of the sequence is

- (a)  $\begin{bmatrix} -4 - j2.5 & j2 & 4 - j2.5 \end{bmatrix}$
- (b)  $\begin{bmatrix} -j2.5 & 1 & j2.5 \end{bmatrix}$
- (c)  $\begin{bmatrix} -j5 & j2 & 0 \end{bmatrix}$
- (d)  $\begin{bmatrix} -4 & 1 & 4 \end{bmatrix}$

63. A casual LTI system is described by the difference equation

$$2y[n] = ay[n-2] - 2x[n] + bx[n-1]$$

the system is stable only if

- (a)  $|a| = 2, |b| < 2$
- (b)  $|a| > 2, |b| > 2$
- (c)  $|a| < 2, \text{ any value of } b$
- (d)  $|b| < 2, \text{ any value of } a$

64. A causal system having the transfer function  $H(s) = \frac{1}{s+2}$  is excited with  $10u(t)$ . The time at which the output reaches 99% of its steady state value is

- (a) 2.7 sec                      (b) 2.5 sec                      (c) 2.4 sec                      (d) 2.1 sec

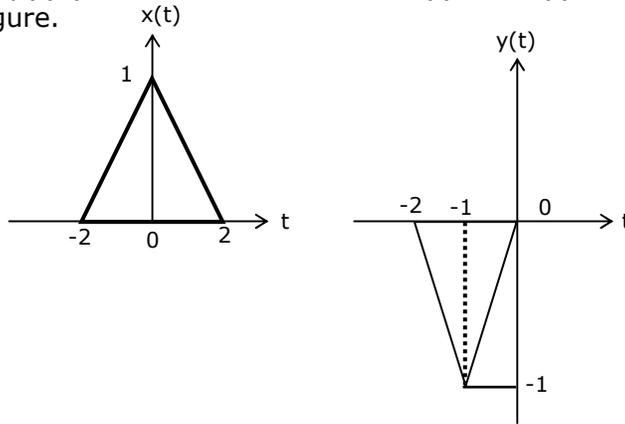
65. The impulse response  $h[n]$  of a linear time invariant system is given as

$$h[n] = \begin{cases} -2\sqrt{2} & n = 1, -1 \\ 4\sqrt{2} & n = 2, -2 \\ 0, & \text{otherwise} \end{cases}$$

If the input to the above system is the sequence  $e^{\frac{jp\pi n}{4}}$ , then the output is

- (a)  $4\sqrt{2}e^{\frac{jp\pi n}{4}}$                       (b)  $4\sqrt{2}e^{-\frac{jp\pi n}{4}}$                       (c)  $4e^{\frac{jp\pi n}{4}}$                       (d)  $-4e^{\frac{jp\pi n}{4}}$

66. Let  $x(t)$  and  $y(t)$  (with Fourier transforms  $X(f)$  and  $Y(f)$  respectively) be related as shown in Figure.



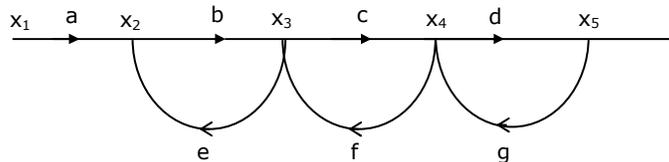
Then  $Y(f)$  is

- (a)  $-\frac{1}{2} X\left(\frac{af}{2b}\right) e^{-j2pf}$                       (b)  $-\frac{1}{2} X\left(\frac{af}{2b}\right) e^{j2pf}$                       (c)  $-X\left(\frac{af}{2b}\right) e^{-j2pf}$                       (d)  $-X\left(\frac{af}{2b}\right) e^{j2pf}$

67. A system has poles at 0.01 Hz, 1 Hz and 80 Hz; zeros at 5 Hz, 100 Hz and 200 Hz. The approximate phase of the system response at 20 Hz is

- (a)  $-90^\circ$                       (b)  $0^\circ$                       (c)  $90^\circ$                       (d)  $-180^\circ$

68. Consider the signal flow graph shown in Figure. The gain  $\frac{X_5}{X_1}$  is

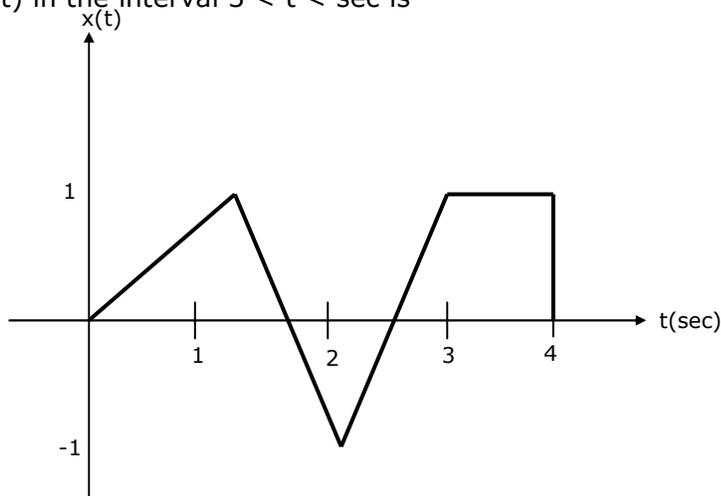


- (a)  $\frac{1 - (be + cf + dg)}{abc}$                       (b)  $\frac{bedg}{1 - (be + cf + dg)}$

- (c)  $\frac{abcd}{1 - (be + cf + dg) + bedg}$                       (d)  $\frac{1 - (be + cf + dg) + bedg}{abcd}$
69. If  $A = \begin{bmatrix} 2 & 2 \\ 1 & -3 \end{bmatrix}$  then  $\sin At$  is
- (a)  $\frac{1}{3} \begin{bmatrix} \sin(-4t) + 2\sin(-t) & -2\sin(-4t) + 2\sin(-t) \\ \sin(-4t) + \sin(-t) & 2\sin(-4t) + \sin(-t) \end{bmatrix}$
- (b)  $\begin{bmatrix} \sin(-2t) & \sin(2t) \\ \sin(t) & \sin(-3t) \end{bmatrix}$
- (c)  $\frac{1}{3} \begin{bmatrix} \sin(4t) + 2\sin(t) & 2\sin(-4t) + 2\sin(-t) \\ \sin(-4t) + \sin(t) & 2\sin(4t) + \sin(t) \end{bmatrix}$
- (d)  $\frac{1}{3} \begin{bmatrix} \cos(-t) + 2\cos(t) & -2\cos(-4t) + 2\sin(-t) \\ \cos(-4t) + \sin(-t) & -2\cos(-4t) + \cos(-t) \end{bmatrix}$
70. The open loop transfer function of a unity feedback system is  $G(s) = \frac{K}{s(s^2 + s + 2)(s + 3)}$ . The range of K for which the system is stable is
- (a)  $\frac{21}{44} > K > 0$                       (b)  $13 > K > 0$                       (c)  $\frac{21}{4} < K < \infty$                       (d)  $-6 < K < \infty$
71. For the polynomial  $P(s) = s^5 + s^4 + 2s^3 + 2s^2 + 3s + 15$ , the number of roots which lie in the right half of the s-plane is
- (a) 4                      (b) 2                      (c) 3                      (d) 1
72. The state variable equations of a system are:
1.  $\dot{x}_1 = -3x_1 - x_2 + u$
  2.  $\dot{x}_2 = 2x_1$
- $y = x_1 + u$
- the system is
- (a) controllable but not observable                      (b) observable but not controllable
- (c) neither controllable nor observable                      (d) controllable and observable
73. Given  $A = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$  the state transition matrix  $e^{At}$  is given by
- (a)  $\begin{bmatrix} e^0 & e^{-t} \\ e^{-t} & 0 \end{bmatrix}$                       (b)  $\begin{bmatrix} e^t & 0 \\ e^0 & e^t \end{bmatrix}$                       (c)  $\begin{bmatrix} e^{-t} & 0 \\ e^0 & e^{-t} \end{bmatrix}$                       (d)  $\begin{bmatrix} e^0 & e^t \\ e^t & 0 \end{bmatrix}$

74. Consider the signal  $x(t)$  shown in Fig.Q.74. Let  $h(t)$  denote the impulse response of the filter matched to  $x(t)$ , with  $h(t)$  being non-zero only in the interval 0 to 4 sec. The slope of  $h(t)$  in the interval  $3 < t < 4$  sec is

- (a)  $\frac{1}{2} \text{ sec}^{-1}$   
 (b)  $-1 \text{ sec}^{-1}$   
 (c)  $-\frac{1}{2} \text{ sec}^{-1}$   
 (d)  $1 \text{ sec}^{-1}$

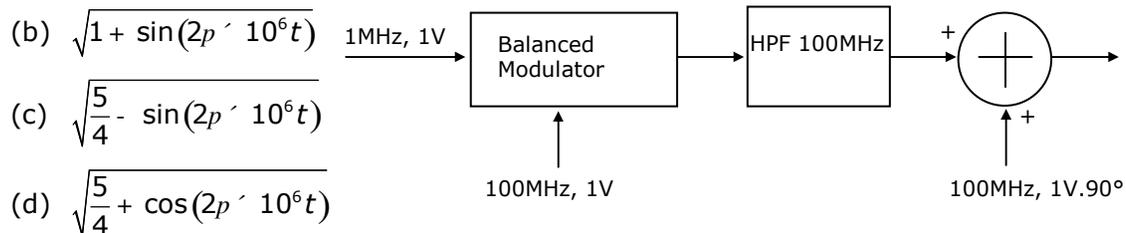


75. A 1mW video signal having a bandwidth of 100 MHz is transmitted to a receiver through a cable that has 40 dB loss. If the effective one-sided noise spectral density at the receiver is  $10^{-20}$  Watt/Hz, then the signal to noise ratio at the receiver is

- (a) 50 db                      (b) 30 db                      (c) 40 db                      (d) 60 db

76. A 100 MHz carrier of 1 V amplitude and a 1 MHz modulating signal of 1 V amplitude are fed to a balanced modulator. The output of the modulator is passed through an ideal high-pass filter with cut-off frequency of 100 MHz. The output of the filter is added with 100 MHz signals of 1 V amplitude and  $90^\circ$  phase shift as shown in Fig.Q.76. The envelope of the resultant signal is

- (a) constant



- (b)  $\sqrt{1 + \sin(2\pi \cdot 10^6 t)}$   
 (c)  $\sqrt{\frac{5}{4} - \sin(2\pi \cdot 10^6 t)}$   
 (d)  $\sqrt{\frac{5}{4} + \cos(2\pi \cdot 10^6 t)}$

77. Two sinusoidal signals of same amplitude and frequencies 10 kHz and 10.1 kHz are added together. The combined signal is given to an ideal frequency detector. The output of the detector is

- (a) 0.1 kHz sinusoid                      (b) 20.1 kHz sinusoid  
 (c) a linear function of time                      (d) a constant

78. Consider a binary digital communication system with equally likely 0's and 1's. When binary 0 is transmitted the voltage at the detector input can lie between the level  $-0.25V$  and  $+0.25V$  with equal probability: when binary 1 is transmitted, the voltage at the detector can have any value between 0 and 1 V with equal probability. If the detector has a threshold of  $2.0V$  (i.e., if the received signal is greater than  $0.2 V$ , the bit is taken as 1), the average bit error probability is

- (a) 0.15                      (b) 0.2                      (c) 0.05                      (d) 0.5

79. A random variable  $X$  with uniform density in the interval 0 to 1 is quantized as follows:

If  $0 \leq X \leq 0.3$ ,               $x_q = 0$

If  $0.3 < X \leq 1$ ,               $x_q = 0.7$

Where  $x_q$  is the quantized value of  $X$

The root-mean square value of the quantization noise is

- (a) 0.573                      (b) 0.198                      (c) 2.205                      (d) 0.266

80.

| Group 1 | Group 2              |
|---------|----------------------|
| 1. FM   | P. Slope overload    |
| 2. DM   | Q. $\mu$ -law        |
| 3. PSK  | R. Envelope detector |
| 4. PCM  | S. Capture effect    |
|         | T. Hilbert transform |
|         | U. Matched filter    |

- (a) 1 - T 2 - P 3 - U 4 - S                      (b) 1 - S 2 - U 3 - P 4 - T  
(c) 1 - S 2 - P 3 - U 4 - Q                      (d) 1 - U 2 - R 3 - S 4 - Q

81. Three analog signals, having bandwidths 1200 Hz, 600 Hz and 600 Hz, are sampled at their respective Nyquist rates, encoded with 12 bit words, and time division multiplexed. The bit rate for the multiplexed signal is

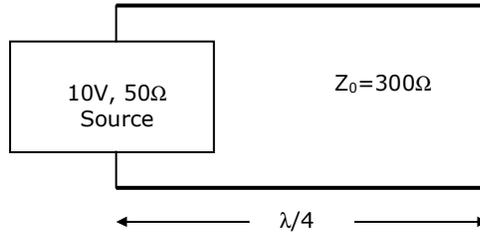
- (a) 115.2 kbps              (b) 28.8 kbps              (c) 57.6 kbps              (d) 38.4 kbps



requirements of BPSK and QPSK respectively. Assuming that the bandwidth of the above rectangular pulses is 10 kHz,  $B_1$  and  $B_2$  are

- (a)  $B_1 = 20$  kHz,  $B_2 = 20$  kHz                      (b)  $B_1 = 10$  kHz,  $B_2 = 20$  kHz  
 (c)  $B_1 = 20$  kHz,  $B_2 = 10$  kHz                      (d)  $B_1 = 10$  kHz,  $B_2 = 10$  kHz

85. Consider a  $300\Omega$  quarter-wave long (at 1 GHz) transmission line as shown in Figure. It is connected to a 10V,  $50\Omega$  sources at one end and is left open circuited at the other end. The magnitude of the voltage at the open circuit end of the line is



- (a) 10 V                      (b) 5 V                      (c) 60 V                      (d)  $\frac{60}{7}$  V

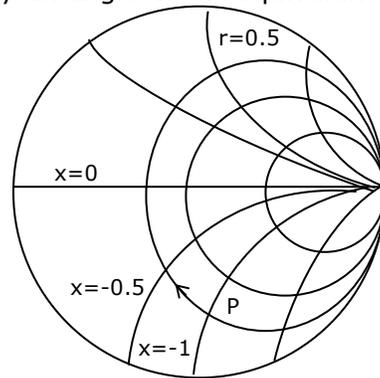
86. In a microwave test bench, why is the microwave signal amplitude modulated at 1 kHz

- (a) To increase the sensitivity of measurement  
 (b) To transmit the signal to a far-off place  
 (c) To study amplitude modulation  
 (d) Because crystal detector fails at microwave frequencies.

87. If  $\vec{E} = (\hat{a}_x + j\hat{a}_y)e^{jkz - j\omega t}$  and  $\vec{H} = \frac{\omega k}{2\omega\mu_0}(\hat{a}_y + j\hat{a}_x)e^{jkz - j\omega t}$ , the time averaged Poynting vector is

- (a) null vector                      (b)  $\frac{\omega k}{2\omega\mu_0}\hat{a}_z$                       (c)  $\frac{\omega k}{\omega\mu_0}\hat{a}_z$                       (d)  $\frac{\omega k}{\omega\mu_0}\hat{a}_z$

88. Consider an impedance  $Z = R + jX$  marked with point P in an impedance Smith chart as shown in Fig.Q.88. The movement from point P along a constant resistance circle in the clockwise direction by an angle  $45^\circ$  is equivalent to



- (a) adding an inductance in series with Z  
 (b) adding a capacitance in series with Z

