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## Section-I: General Ability

1. Seven machines take 7 minutes to make 7 identical toys. At the same rate, how many minutes would it take for 100 machines to make 100 toys?
(A) 1
(B) 7
(C) 100
(D) 700

Key: (B)
Sol: $\quad \frac{7 \times 7}{7}=\frac{100 \times \mathrm{T}_{2}}{100}$
$\Rightarrow \mathrm{T}_{2}=7$ minutes
2. "Her $\qquad$ should not be confused with miserliness; she is ever willing to assist those in need."

The word that best fills the blank in the above sentence is:
(A) cleanliness
(B) punctuality
(C) frugality
(D) greatness

## Key: (C)

Sol: The sentence explains that the person spoken of is not miserly, since she is quite prepared to be generous. So for the sentence to make sense, the word filling the blank has to be something that is consistent with generosity and yet might, by those without a full understanding of her behaviour, be mistaken for miserliness. The words "frugality" and thrift fulfill this requirement and yield two sentences that are alike in meaning. Thus the correct answer is frugality.
3. A number consists of two digits. The sum of the digits is 9 . If 45 is subtracted from the number, its digits are interchanged. What is the number?
(A) 63
(B) 72
(C) 81
(D) 90

Key: (B)
Sol: Let number be ' $x y$ '
Given $x+y=9$
$\& x y-45=y x$
$\downarrow$
$\Rightarrow(10 x+y)-45=10 y+x$
$\Rightarrow 9 x-9 y=45$
$\Rightarrow \mathrm{x}-\mathrm{y}=5$
solving (i) \& (ii) $\Rightarrow \mathrm{x}=7, \mathrm{y}=2$
Required number $=72$
4. Going by the $\qquad$ that many hands make light work, the school $\qquad$ involved all the students in the task."
(A) principle, principal
(B) principal, principle
(C) principle, principle
(D) principal, principal

Key: (A)
5. A rectangle becomes a square when its length and breadth are reduced by 10 m and 5 m , respectively. During this process, the rectangle loses $650 \mathrm{~m}^{2}$ of area. What is the area of the original rectangle in square meters?
(A) 1125
(B) 2250
(C) 2924
(D) 4500

Key: (B)
Sol:

X


Area of rectangle $=(x+10)(x+5)=x^{2}+15 x+50$
Area of square $=x^{2}$
By the given condition,

$$
15 x+50=650
$$

$\Rightarrow 15 \mathrm{x}=600 \Rightarrow \mathrm{x}=40$.
$\therefore$ Area of rectangle $=(40)^{2}+15 \times 40+50=2250(\because$ from $(1))$
6. Given that $a$ and $b$ are integers and $a+a^{2} b^{3}$ is odd, which one of the following statements is correct?
(A) $a$ and $b$ are both odd
(B) a and bare both even
(C) a is even and $b$ is odd
(D) $a$ is odd and $b$ is even

Key: (D)
Sol: By verifying options
Let us consider $\mathrm{a}=1, \mathrm{~b}=2$
$\mathrm{a}+\mathrm{a}^{2} \mathrm{~b}^{3}=1+1^{2} \times 2^{3}=9$ i.e., odd
Only this condition is valid.
7. Consider the following three statements:
(i) Some roses are red
(ii) All red flowers fade quickly.
(iii) Some roses fade quickly

Which of the following statements can be logically inferred from the above statements?
(A) If (i) is true and (ii) is false, then (iii) is false.
(B) If (i) is true and (ii) is false, then (iii) is true.
(C) If (i) and (ii) are true, then (iii) is true.
(D) If (i) and (ii) are false, then (iii) is false.

Key: (C)
Sol:

8. Which of the following functions describe the graph shown in the below figure.

(A) $\mathrm{y}=||\mathrm{x}|+1|-2$
(B) $y=||x|-1|-1$
(C) $y=||x|+1|-1$
(D) $y=|x-1|-1 \mid$

Key: (B)
Sol: Given graph passing through X -axis at $\mathrm{x}=-2,2$
From option (B), $\mathrm{y}=0$ at $\mathrm{x}=-2,2$
Alternate Method:
Step (1)
$y=|x|$


$$
\begin{aligned}
& \operatorname{Step}(2) \\
& y+1=|x| \\
& (\text { or }) \\
& y=|x|-1
\end{aligned}
$$



$$
\begin{aligned}
& \operatorname{Step}(3) \\
& y=|x|-1 \mid
\end{aligned}
$$

$$
\operatorname{Step}(4)
$$

$$
y+1=||x|-1|
$$

(or)

$$
\mathrm{y}=||\mathrm{x}|-1|-1
$$

9. From the time the front of a train enters a platform, it takes 25 seconds for the back of the train to leave the platform, while travelling at a constant speed of $54 \mathrm{~km} / \mathrm{h}$. At the same speed, it takes 14 seconds to pass a man running at $9 \mathrm{~km} / \mathrm{h}$ in the same directions as the train. What is the length of the train and that of the platform in meters, respectively?
(A) 210 and 140
(B) 162.5 and 187.5
(C) 245 and 130
(D) 175 and 200

Key: (D)
Sol: Let Train length $=x$

$$
\text { Platform length }=y
$$

$\{\mathrm{x}+\mathrm{y}\}=\{25\} \times\left(54 \times \frac{5}{18}\right)=375$
$\stackrel{\text { Distance }}{\downarrow}=\stackrel{\text { Time }}{\downarrow} \times \underset{\text { Speed }}{\downarrow}$
also, $\frac{x}{\substack{(54-9) \times \frac{5}{18} \\ \downarrow}}=14$
Relative speed
$\Rightarrow \mathrm{x}=175$ and $\mathrm{y}=200$
10. For integers $a, b$ and $c$, what would be the minimum and maximum values respectively of $a+b+c$ if $\log |a|+\operatorname{lob}|b|+\log |c|=0$ ?
(A) -3 and 3
(B) - 1 and 1
(C) - 1 and 3
(D) 1 and 3

Key: (A)
Sol: $\quad$ Given $\log |a|+\log |b|+\log |c|=0$
$\Rightarrow \log _{\mathrm{e}}|\mathrm{a}||\mathrm{b}||\mathrm{c}|=0$
$\Rightarrow|\mathrm{a}||\mathrm{b}||\mathrm{c}|=1 \Rightarrow \mathrm{a}= \pm 1, \mathrm{~b}= \pm 1, \mathrm{c}= \pm 1 \quad(\because \mathrm{a}, \mathrm{b}, \mathrm{c}$ are integers $)$
Minimum value $=-1-1-1=-3$
Maximum value $=1+1+1=3$

## Section-I: Mechanical Engineering

1. An ideal gas undergoes a process from state $1\left(\mathrm{~T}_{1}=300 \mathrm{~K}, \mathrm{p}_{1}=100 \mathrm{kPa}\right)$ to state $2\left(\mathrm{~T}_{2}=600 \mathrm{~K}\right.$, $\left.\mathrm{p}_{2}=500 \mathrm{kPa}\right)$. The specific heats of the ideal gas are: $\mathrm{c}_{\mathrm{p}}=1 \mathrm{~kJ} / \mathrm{kg}-\mathrm{K}$ and $\mathrm{c}_{\mathrm{v}}=0.7 \mathrm{~kJ} / \mathrm{kgK}$. The change in specific entropy of the ideal gas from state 1 to state 2 (in $\mathrm{kJ} / \mathrm{kg}-\mathrm{K}$ ) is $\qquad$ (correct to two decimal places).
Key: (0.21)
Sol: Given that,
$\mathrm{T}_{1}=300 \mathrm{~K}, \mathrm{P}_{1}=100 \mathrm{kPa}$
$\mathrm{T}_{2}=600 \mathrm{~K}, \mathrm{P}_{2}=500 \mathrm{kPa}$
$\mathrm{C}_{\mathrm{p}}=1 \mathrm{~kJ} / \mathrm{kg}-\mathrm{k}$
$\mathrm{C}_{\mathrm{v}}=0.7 \mathrm{~kJ} / \mathrm{kg}-\mathrm{k}$,
$\mathrm{R}=\mathrm{C}_{\mathrm{p}}-\mathrm{C}_{\mathrm{v}}=1-0.7=0.3 \mathrm{~kJ} / \mathrm{kg}-\mathrm{k}$
Changein Entropy $\left(\mathrm{s}_{2}-\mathrm{s}_{1}\right)$ per unit mass
$=C_{p} \ln \left(\frac{T_{2}}{T_{1}}\right)-R \ln \left(\frac{\mathrm{P}_{2}}{\mathrm{P}_{1}}\right)$
$=1 \ln \left(\frac{600}{300}\right)-0.3 \ln \left(\frac{500}{100}\right)$
$\mathrm{s}_{2}-\mathrm{s}_{1}=0.21 \mathrm{~kJ} / \mathrm{kg}-\mathrm{K}$
2. In a linearly hardening plastic material, the true stress beyond initial yielding
(A) increases linearly with the true strain
(B) decreases linearly with the true strain
(C) first increases linearly and then decreases linearly with the true strain
(D) remain constant

Key: (A)
3. Using the Taylor's tool life equation with exponent $\mathrm{n}=0.5$, if the cutting speed is reduced by $50 \%$, the ratio of new tool life to original tool life is
(A) 4
(B) 2
(C) 1
(D) 0.5

Key: (A)
Sol: $\quad \mathrm{VT}^{\mathrm{n}}=\mathrm{C}$
$\mathrm{V}_{1} \mathrm{~T}_{1}^{\mathrm{n}}=\mathrm{V}_{2} \mathrm{~T}_{2}^{\mathrm{n}}$
$\frac{\mathrm{T}_{2}}{\mathrm{~T}_{1}}=\left(\frac{\mathrm{V}_{1}}{\mathrm{~V}_{2}}\right)^{\frac{1}{n}}$
$\frac{\mathrm{T}_{2}}{\mathrm{~T}_{1}}=\left(\frac{\mathrm{V}_{1}}{0.5 \mathrm{~V}_{1}}\right)^{\frac{1}{0.5}} \quad\left(\because \mathrm{~V}_{2}=0.5 \mathrm{~V}_{1}\right)$
$\mathrm{T}_{2}=4 \mathrm{~T}_{1}$
4. The height (in mm ) for a 125 mm sine bar to measure a taper of $27^{\circ} 32^{\prime}$ on a flat work piece is $\qquad$
$\qquad$ (correct to three decimal places).

Key: (57.77)
Sol: $\theta=27^{\circ} 32^{\prime}=27.53^{\circ}$
$\because \sin \theta=\frac{\mathrm{h}}{\ell}$
$\mathrm{h}=\ell \sin \theta=(25 \sin 27.53)=57.77 \mathrm{~mm}$
5. A six-faced fair dice is rolled five times. The probability (in \%) of obtaining "ONE" at least four times is
(A) 33.3
(B) 3.33
(C) 0.33
(D) 0.0033

## Key: (C)

Sol: $\quad \mathrm{n}=5, \mathrm{p}\left(\right.$ obtaining $\left.^{\prime} \mathrm{ONE}^{\prime}\right)=\frac{1}{6}$
$\Rightarrow \mathrm{q}=1-\frac{1}{6}=\frac{5}{6}$
$p(x \geq 4)=$ ?
By Binomial distribution,

$$
\begin{aligned}
\mathrm{p}(\mathrm{x} \geq 4) & =\mathrm{p}(\mathrm{x}=4)+\mathrm{p}(\mathrm{x}=5) \\
& ={ }^{5} \mathrm{C}_{4}\left(\frac{1}{6}\right)^{4}\left(\frac{5}{6}\right)^{5-4}+{ }^{5} \mathrm{C}_{5}\left(\frac{1}{6}\right)^{5}\left(\frac{5}{6}\right)^{5-5} \\
& =\frac{26}{6^{5}}=\frac{26}{6^{5}} \times 100(\text { in } \%) \simeq 0.33
\end{aligned}
$$

6. The time series forecasting method that gives equal weightage to each of the m most recent observations is
(A) Moving average method
(B) Exponential smoothing with linear trend
(C) Triple Exponential smoothing
(D) Kalman Filter

Key (A)
Sol $\because$ in Moving Average Method

$$
F_{n+1}=\frac{D_{n}+D_{n-1}+D_{n-2}+\ldots}{n}
$$

So, weightage of all past data is $\frac{1}{n}$
i.e., equal weightage provided to all past data.
7. The rank of the matrix $\left[\begin{array}{ccc}-4 & 1 & -1 \\ -1 & -1 & -1 \\ 7 & -3 & 1\end{array}\right]$ is
(A) 1
(B) 2
(C) 3
(D) 4

Key: (B)
Sol: Let $\mathrm{A}=\left[\begin{array}{ccc}-4 & 1 & -1 \\ -1 & -1 & -1 \\ 7 & -3 & 1\end{array}\right]$
$|\mathrm{A}|=-4(-1-3)-1(-1+7)-(3+7)=0$
consider a $2 \times 2$ sub matrix, $\left|\begin{array}{cc}-4 & 1 \\ -1 & -1\end{array}\right|=4+1=5 \neq 0$
$\Rightarrow$ Rank of $\mathrm{A}=2$
8. Interpolator in a CNC machine
(A) controls spindle speed
(B) coordinates axes movements
(C) operates tool changer
(D) commands canned cycle

Key: (B)
9. Four red balls, four green balls and four blue balls are put in a box. Three balls are pulled out of the box at random one after another without replacement. The probability that all the three balls are red is
(A) $1 / 72$
(B) $1 / 55$
(C) $1 / 36$
(D) $1 / 27$

Key: (B)
Sol: 4-Red; 4-Green; 4-Blue
Required probability $=\frac{4}{12} \times \frac{3}{11} \times \frac{2}{10}=\frac{1}{55}$
10. A grinding ratio of 200 implies that the
(A) grinding wheel wears 200 times the volume of the material removed.
(B) grinding wheel wears 0.005 times the volume of the material removed
(C) aspect ratio of abrasive particles used in the grinding wheel is 200
(D) ratio of volume of abrasive particle to that of grinding wheel is 200

Key: (B)
Sol: $\quad$ Grinding ratio $=\frac{\text { MRR }}{\text { wheel wear }}$

$$
200=\frac{1}{\text { wheel wear }}
$$

wheel wear $=\frac{1}{200}=0.005$
11. Which one of the following statements is correct for a superheated vapour?
(A) Its pressure is less than the saturation pressure at a given temperature.
(B) Its temperature is less than the saturation temperature at a given pressure.
(C) Its volume is less than the volume of the saturated vapour at a given temperature.
(D) Its enthalpy is less than enthalpy of the saturated vapour at a given pressure.

## Key: (A)

Sol: At a given temperature the pressure of superheated vapour is less than the saturation pressure.
For example let us take $100^{\circ} \mathrm{C}$, the saturation pressure corresponding to this temperature is 1.01325 bar. If the saturation pressure decreases saturation temperature decreases and vice-versa. From this we can easily say that if the superheated temperature has to be $100^{\circ} \mathrm{C}$ then saturation temperature should be less than $100^{\circ} \mathrm{C}$, therefore corresponding saturation pressure will be less.

Hence we can say that for same temperature the pressure of superheated vapour is less than the saturation pressure.
12. If $\sigma_{1}$ and $\sigma_{3}$ are the algebraically largest and smallest principal stresses respectively, the value of the maximum shear stress is
(A) $\frac{\sigma_{1}+\sigma_{3}}{2}$
(B) $\frac{\sigma_{1}-\sigma_{3}}{2}$
(C) $\sqrt{\frac{\sigma_{1}+\sigma_{3}}{2}}$
(D) $\sqrt{\frac{\sigma_{1}-\sigma_{3}}{2}}$

Key: (B)
Sol: Diameter of Mohr circle $=\sigma_{1}-\sigma_{3}$ and

$$
\therefore \tau_{\max }=\text { Radius }=\frac{\sigma_{1}-\sigma_{3}}{2}
$$

13. The number of atoms per unit cell and the number of slip systems, respectively, for a face-centered cubic (FCC) crystal are
(A) 3, 3
(B) 3,12
(C) 4,12
(D) 4,48

Key: (C)
14. A four bar mechanism is made up of links of length $100,200,300$ and 350 mm . If the 350 mm link is fixed, the number of links that can rotate fully is $\qquad$ -.

Key: (1)
Sol: $\quad \ell+\mathrm{s}<\mathrm{p}+\mathrm{q}$
$100+350<200+300$
Hence it is crank rocker
(100) link will rotate -1 .


So, link whose length is 100 mm will rotate fully. So, only one link will rotate fully.
15. For an Oldham coupling used between two shafts, which among the following statements are correct?
I. Torsional load is transferred along shaft axis.
II. A velocity ratio of $1: 2$ between shafts is obtained without using gears.
III. Bending load is transferred transverse to shaft axis.
IV. Rotation is transferred along shaft axis.
(A) I and III
(B) I and IV
(C) II and III
(D) II and IV

Key: (B)
16. A flat plate of width $L=1 \mathrm{~m}$ is pushed down with a velocity $U=0.01 \mathrm{~m} / \mathrm{s}$ towards a wall resulting in the drainage of the fluid between the plate and the wall as shown in the figure.


[^0]Assume two-dimensional incompressible flow and that the plate remains parallel to the wall. The average velocity, $u_{\text {avg }}$ of the fluid (in $\mathrm{m} / \mathrm{s}$ ) draining out at the instant shown in the figure is $\qquad$ (correct to three decimal places).

Key: (0.05)
Sol: Let $\mathrm{b}=$ length of plate perpendicular to paper
Volume drain out per sec $=$ L.b.U
So, L.b.U $=2 b . u_{\text {avg }} \cdot d$

$$
\begin{aligned}
& u_{\mathrm{avg}}=\frac{\mathrm{L} . \mathrm{U}}{2 \mathrm{~d}}=\frac{1 \times 0.01}{2 \times 0.1} \\
& u_{\mathrm{avg}}=0.05 \mathrm{~m} / \mathrm{s}
\end{aligned}
$$

17. According to the Mean Value Theorem, for a continuous function $f(x)$ in the interval [a, b], there exists a value $\xi$ in this interval such that $\int_{a}^{b} f(x) d x=$
(A) $\mathrm{f}(\xi)(\mathrm{b}-\mathrm{a})$
(B) $\mathrm{f}(\mathrm{b})(\xi-\mathrm{a})$
(C) $f(a)(b-\xi)$
(D) 0

Key: (A)
Sol: By using mean value theorem for definite integrals,
$\exists \xi f(\mathrm{a}, \mathrm{b})$ s.t $\int_{\mathrm{a}}^{\mathrm{b}} \mathrm{f}(\mathrm{x}) \mathrm{dx}=(\mathrm{b}-\mathrm{a}) \mathrm{f}(\xi)$
$\exists \xi$ in between a \& b s.t
Area of rectangle abcd = Area under the curve $f(x)$ with $x$-axis
i.e., $(b-a) f(\xi)=\int_{a}^{b} f(x) d x$

18. A steel column of rectangular section ( $15 \mathrm{~mm} \times 10 \mathrm{~mm}$ ) and length 1.5 m is simply supported at both ends. Assuming modulus of elasticity, $\mathrm{E}=200 \mathrm{GPa}$ for steel, the critical axial load (in kN ) is ___ (correct to two decimal places)

Key: (1.097)
Sol: $\quad \ell_{\mathrm{e}}=1500 \mathrm{~mm}, \mathrm{~b}=15 \mathrm{~mm}, \mathrm{~d}=10 \mathrm{~mm}, \mathrm{E}=200 \mathrm{GPa}$

$$
\begin{aligned}
& \mathrm{P}_{\mathrm{E}}=\frac{\pi^{2} \mathrm{EI}}{\ell_{\mathrm{e}}{ }^{2}} ; \mathrm{I}=\frac{15 \times 10^{3}}{12} \\
& =\frac{\pi^{2} \times 200 \times 10^{3} \times \frac{15 \times 10^{3}}{12}}{(1500)^{2}}=1.097 \mathrm{kN}
\end{aligned}
$$

19. If the wire diameter of a compressive helical spring is increased by $2 \%$, the change in spring stiffness (in \%) is $\qquad$ (correct to two decimal places.)

Key: (8.243)
Sol: $\mathrm{d}_{2}=1.02 \mathrm{~d}_{1}$
$\mathrm{k}=\frac{\mathrm{Gd}^{4}}{8 \mathrm{WD}^{3}} \Rightarrow \mathrm{k} \propto \mathrm{d}^{4}$
$\frac{\mathrm{k}_{1}}{\mathrm{k}_{2}}=\left(\frac{\mathrm{d}_{1}}{1.02 \mathrm{~d}_{1}}\right)^{4} \Rightarrow \mathrm{k}_{2}=1.082$
$\%$ change in stiffness $=\frac{\mathrm{k}_{2}-\mathrm{k}_{1}}{\mathrm{k}_{1}}=\left(\frac{1.082-1}{1}\right) \times 100 \%=8.243 \%$
20. For a two-dimensional incompressible flow field given by $\overrightarrow{\mathrm{u}}=\mathrm{A}(x \hat{\mathrm{i}}-\mathrm{y} \hat{\mathrm{j}})$, where $A>0$, which one of the following statements is FALSE?
(A) It satisfies continuity equation
(B) It is unidirectional when $\mathrm{x} \rightarrow 0$ and $\mathrm{y} \rightarrow \infty$,
(C) Its streamlines are given by $x=y$.
(D) It is irrotational

Key: (C)
Sol: $\because$ Equation of streamline
$\frac{d y}{d x}=\frac{v}{u}=\frac{-y}{x}$
$\int \frac{d y}{y}=\int-\frac{d x}{x} \Rightarrow \ell n y=\ell n x+\ell n c$
$x y=C . S o$, option C is false.
21. The equation of motion for a spring-mass system excited by a harmonic force is $m \ddot{\mathrm{x}}+K x=\mathrm{F} \cos (\omega \mathrm{t})$,
where $M$ is the mass, $K$ is the spring stiffness, F is the force amplitude and $\omega$ is the angular frequency of excitation. Resonance occurs when $\omega$ is equal to
(A) $\sqrt{\frac{\mathrm{M}}{\mathrm{K}}}$
(B) $\frac{1}{2 \pi} \sqrt{\frac{K}{M}}$
(C) $\quad 2 \pi \sqrt{\frac{\mathrm{~K}}{\mathrm{M}}}$
(D) $\sqrt{\frac{K}{M}}$

Key: (D)

Sol: Resonance will occur when, $\mathrm{r}=1$.
i.e., when $\omega=\omega_{\mathrm{n}}=\sqrt{\frac{\mathrm{K}}{\mathrm{M}}}$
22. A bar of uniform cross section and weighing 100 N is held horizontally using two massless and inextensible strings S1 and S2 as shown in the figure.

Rigid support


The tensions in the strings are
(A) $T_{1}=100 \mathrm{~N}$ and $T_{2}=0 \mathrm{~N}$
(B) $T_{1}=0 \mathrm{~N}$ and $T_{2}=100 \mathrm{~N}$
(C) $T_{1}=75 \mathrm{~N}$ and $T_{2}=25 \mathrm{~N}$
(D) $T_{1}=25 \mathrm{~N}$ and $T_{2}=75 \mathrm{~N}$

Key: (B)
Sol: $\quad \Sigma \mathrm{M}_{\mathrm{A}}=0$
$\mathrm{T}_{2} \times \frac{\mathrm{L}}{2}=100 \times \frac{\mathrm{L}}{2}$
$\mathrm{T}_{2}=100$
$\mathrm{T}_{1}+\mathrm{T}_{2}=100$
$\mathrm{T}_{1}=0 \mathrm{~N}, \mathrm{~T}_{2}=100 \mathrm{~N}$

23. $F(z)$ is a function of the complex variable $z=x+i y$ given by

$$
F(z)=i z+k \operatorname{Re}(z)+\mathrm{i} \operatorname{Im}(z)
$$

For what value of k will $F(z)$ satisfy the Cauchy-Riemann equations?
(A) 0
(B) 1
(C) -1
(D) $y$

Key: (B)
Sol: $\quad \mathrm{F}(\mathrm{z})=\mathrm{iz}+\mathrm{kRe}(\mathrm{z})+\mathrm{iI}_{\mathrm{m}}(\mathrm{z})$

$$
\begin{aligned}
& =i(x+i y)+k x+i y \\
& =i x-y+k x+i y \\
& =(k x-y)+i(x+y) \\
& =u+i v(\text { say })
\end{aligned}
$$

Applying C-R equations, i.e., $\frac{\partial u}{\partial x}=\frac{\partial v}{\partial y} \& \frac{\partial u}{\partial y}=\frac{\partial v}{\partial x} \Rightarrow k=1$
24. The type of weld represented by the shaded region in the figure is

(A) groove
(B) spot
(C) fillet
(D) plug

Key: (C)
25. For a Pelton wheel with a given water jet velocity, the maximum output power from the Pelton wheel is obtained when the ratio of the bucket speed to the water jet speed is $\qquad$ (correct to two decimal places).
Key: (0.5)
Sol: $\because$ Efficiency of Pelton wheel is maximum,
when $\frac{\mathrm{u}}{\mathrm{v}}=0.5$
Where $u=$ velocity of blade
$\mathrm{v}=$ velocity of jet (Absolute) at inlet.
26. Let $\mathrm{X}_{1}, \mathrm{X}_{2}$ be two independent normal random variables with means $\mu_{1}, \mu_{2}$ and standard deviations $\sigma_{1}, \sigma_{2}$ respectively. Consider $Y=\mathrm{X}_{1}-\mathrm{X}_{2} ; \mu_{1}=\mu_{2}=1, \sigma_{1}=1, \sigma_{2}=2$, Then,
(A) Y is normal distributed with mean 0 and variance 1
(B) Y is normally distributed with mean 0 and variance 5
(C) Y has mean 0 and variance 5, but is NOT normally distributed
(D) Y has mean 0 and variance 1, but is NOT normally distributed

Key: (B)
Sol: Sum or difference of normal random variables is again a normal random variable

$$
\begin{aligned}
\text { Mean of ' } \mathrm{y} \text { ' }=\mathrm{E}(\mathrm{y})=\mathrm{E}\left(\mathrm{x}_{1}-\mathrm{x}_{2}\right) & =\mathrm{E}\left(\mathrm{x}_{1}\right)-\mathrm{E}\left(\mathrm{x}_{2}\right) \\
& =\mu_{1}-\mu_{2} \\
& =1-1=0 \\
\text { Variance of ' } \mathrm{y} \text { ' }=\mathrm{v}(\mathrm{y})=\mathrm{v}\left(\mathrm{x}_{1}-\mathrm{x}_{2}\right) & =\mathrm{v}\left(\mathrm{x}_{1}\right)+\mathrm{v}\left(\mathrm{x}_{2}\right) \\
& =\sigma_{1}^{2}+\sigma_{2}^{2} \\
& =1+4=5
\end{aligned}
$$

27. A slider crank mechanism is shown in the figure. At some instant, the crank angle is $45^{\circ}$ and a force of 40 N is acting towards the left on the slider. The length of the crank is 30 mm and the connecting rod is 70 mm . Ignoring the effect of gravity, friction and inertial forces, the magnitude of the crankshaft torque (in Nm ) needed to keep the mechanism in equilibrium is $\qquad$ (correct to two decimal places).


Key: (1.117)
Sol: $\quad \mathrm{F}_{\mathrm{p}}=40 \mathrm{~N}$
$30 \sin 45^{\circ}=70 \sin \phi$
$\sin \phi=0.303 \Rightarrow \phi=17.6^{\circ}$
Torque $=\frac{\mathrm{F}_{\mathrm{p}}}{\cos \phi} \sin (\theta+\phi) \times \mathrm{r}$

$=\frac{40 \times \sin \left(17.6+45^{\circ}\right)}{\cos 17.6} \times 0.03=1.117 \mathrm{~N}-\mathrm{mts}$


Key: (33.89)
Sol: For the steady state heat transfer,

$\Rightarrow \mathrm{T}_{\mathrm{p}}=33.89^{\circ} \mathrm{C}$, So answer is 33.89
30. $\mathrm{F}(\mathrm{s})$ is the Laplace transform of the function

$$
f(t)=2 t^{2} e^{-t}
$$

$F(1)$ is $\qquad$ (correct to two decimal places).

Key: (0.5)
Sol: $\quad L\left(2 t^{2} e^{-t}\right)=2 L\left[t^{2} e^{-t}\right]$

$$
\begin{aligned}
& =2 \times \frac{2}{(\mathrm{~s}+1)^{3}}\left(\because \mathrm{~L}\left[\mathrm{t}^{2}\right]=\frac{2!}{\mathrm{s}^{3}}=\frac{2}{\mathrm{~s}^{3}} \& \mathrm{~L}\left[\mathrm{e}^{-\mathrm{at}} \mathrm{f}(\mathrm{t})=\mathrm{F}(\mathrm{~s}+\mathrm{a})\right]\right) \\
& =\frac{4}{(\mathrm{~s}+1)^{3}}=\mathrm{F}(\mathrm{~s}) \\
\Rightarrow \mathrm{F}(1)= & \frac{4}{8}=0.5
\end{aligned}
$$

31. The true stress $(\sigma)$ - true strain $(\varepsilon)$ diagram of a strain hardening material is shown in figure. First, there is loading up to point A, i.e. up to stress of 500 MPa and strain of 0.5 . Then from point A , there is unloading up to point $B$, i.e., to stress of 100 MPa , Given that the Young's modulus $E=200 \mathrm{GPa}$, the natural strain at point B ( $\varepsilon_{B}$ ) $\qquad$ (correct to two decimal places).


Exp: (0.498)
Sol: $\quad \because \mathrm{E}=$ slope $=\frac{\mathrm{AC}}{\mathrm{BC}}$
$200 \times 10^{9}=\frac{400 \times 10^{6}}{\mathrm{BC}} \Rightarrow \mathrm{BC}=2 \times 10^{-3}=0.002$

32. The percentage scrap in a sheet metal blanking operation of a continuous strip of sheet metal as shown in the figure is $\qquad$ (correct to two decimal places).


Key: (53.27)
Sol: Area of rectangle

$$
\mathrm{ABCD}=\frac{6 \mathrm{D}}{5} \times \frac{7 \mathrm{D}}{5}=\frac{42}{25} \mathrm{D}^{2}=1.68 \mathrm{D}^{2}
$$

Area of blank $=\frac{\pi}{4} D^{2}=0.785 D^{2}$
So, $\%$ scrap $=\frac{1.68 \mathrm{D}^{2}-0.785 \mathrm{D}^{2}}{1.68 \mathrm{D}^{2}} \times 100=53.27 \%$

$D+\frac{D}{5}=\frac{6 D}{5}$
33. An epicyclic gear train is shown in the figure below. The number of teeth on the gears $A, B$ and $D$ are 20, 30 and 20 respectively. Gear $C$ has 80 teeth on the inner surface and 100 teeth on the outer surface. If the carrier arm $A B$ is fixed and the sun gear $A$ rotates at 300 rpm in the clockwise direction, then the rpm of $D$ in the clockwise direction is
(A) 240
(B) -240
(C) 375
(D) -375


Key: (C)
Sol: $\quad \mathrm{N}_{\mathrm{A}}=300 \mathrm{rpm} ; \mathrm{T}_{\mathrm{A}}=20 ; \mathrm{T}_{\mathrm{B}}=30 ; \mathrm{T}_{\mathrm{c}_{\mathrm{in}}}=80$
$\mathrm{T}_{\mathrm{c}_{\mathrm{ett}}}=100$
$\mathrm{N}_{\mathrm{B}}=\frac{\mathrm{N}_{\mathrm{A}} \mathrm{T}_{\mathrm{A}}}{\mathrm{T}_{\mathrm{B}}}=\frac{300 \times 20}{30}=200$
$\mathrm{N}_{\mathrm{C}}=\frac{\mathrm{N}_{\mathrm{B}} \mathrm{T}_{\mathrm{B}}}{\mathrm{T}_{\mathrm{C}}}=\frac{200 \times 30}{80}=75$
$\mathrm{N}_{\mathrm{D}}=\frac{\mathrm{N}_{\mathrm{C}} \mathrm{T}_{\mathrm{C}}}{\mathrm{T}_{\mathrm{D}}}=\frac{75 \times 100}{20}=375 \mathrm{rpm}$
34. The minimum value of $3 x+5 y$ such that:
$3 x+5 y \leq 15$
$4 x+9 y \leq 8$
$13 x+2 y \leq 2$
$x \geq 0, y \geq 0$
is $\qquad$ .

Key: (0)
Sol: $\because$ All main constraints are of $\leq$ type and
Non-negativity constraints are of $\geq$ type.
So, feasible region contain origin $(0,0)$ as corner point.
So, at origin $(0,0)$
$\mathrm{z}_{\text {min }}=3 \times 0+5 \times 0=0$
35. Block P of mass 2 kg slides down the surface and has a speed $20 \mathrm{~m} / \mathrm{s}$ at the lowest point, Q , where the local radius of curvature is 2 m as shown in the figure. Assuming $\mathrm{g}=10 \mathrm{~m} / \mathrm{s}^{2}$, the normal force (in N ) at Q is $\qquad$ (correct to two decimal places).


Key: (420)
Sol: $\quad R_{Q}=m g+\frac{\mathrm{mv}^{2}}{\mathrm{R}}$

$$
=(2 \times 10)+\left(\frac{2 \times 20^{2}}{2}\right)=20+400=420 \mathrm{~N}
$$

36. A solid block of 2.0 kg mass slides steadily at a velocity $V$ along a vertical wall as shown in the figure below. A thin oil film of thickness $h=0.15 \mathrm{~mm}$ provides lubrication between the block and the wall. The surface area of the face of the block in contact with the oil film is $0.04 \mathrm{~m}^{2}$. The velocity distribution within the oil film gap is linear as shown in the figure. Take dynamic viscosity of oil as $7 \times 10^{-3} \mathrm{~Pa}-\mathrm{s}$ and acceleration due to gravity as $10 \mathrm{~m} / \mathrm{s}^{2}$. Neglect weight of the oil. The terminal velocity V (in $\mathrm{m} / \mathrm{s}$ ) of the block is $\qquad$ (correct to one decimal place).


Key: (10.714)
Sol: $\quad \because \mathrm{F}=\tau$.A

$$
\begin{aligned}
& \mathrm{F}=\mu\left(\frac{\mathrm{du}}{\mathrm{dy}}\right) \cdot \mathrm{A} \Rightarrow \mathrm{~F}=\mu \cdot \frac{\mathrm{V}}{\mathrm{~h}} \cdot \mathrm{~A} \\
& \Rightarrow 2 \times 10=7 \times 10^{-3} \times \frac{\mathrm{V}}{0.15 \times 10^{-3}} \times 0.04
\end{aligned}
$$

$$
\Rightarrow \mathrm{V}=10.714 \mathrm{~m} / \mathrm{s}
$$

37. A machine of mass $m=200 \mathrm{~kg}$ is supported on two mounts, each of stiffness $\mathrm{k}=10 \mathrm{kN} / \mathrm{m}$. The machine is subjected to an external force (in N ) $\mathrm{F}(\mathrm{t})=50 \cos 5 \mathrm{t}$. Assuming only vertical translatory motion, the magnitude of the dynamic force (in N ) transmitted from each mount to the ground is
$\qquad$ (correct to two decimal places).


Key: (33.33)
Sol: $\mathrm{k}=10 \mathrm{kN} / \mathrm{m}, \mathrm{m}=200 \mathrm{~kg}$
$\mathrm{F}=50 \cos 5 \mathrm{t}, \omega=5 \mathrm{rad} / \mathrm{sec}$
$\mathrm{F}=50$
$\omega_{\mathrm{n}}=\sqrt{\frac{20000}{200}}=10 \mathrm{rad} / \mathrm{sec}$
$\xi=0$
$\epsilon=\frac{\mathrm{F}_{\mathrm{T}}}{\mathrm{F}}=\frac{\sqrt{1+(2 \xi \mathrm{r})^{2}}}{\sqrt{\left(1-\mathrm{r}^{2}\right)^{2}+(2 \xi \mathrm{r})^{2}}}$
$\frac{\mathrm{F}_{\mathrm{T}}}{50}=\frac{1}{1-\left(\frac{5}{10}\right)^{2}}$
$\frac{\mathrm{F}_{\mathrm{T}}}{50}=\frac{1}{\left(\frac{3}{4}\right)} \Rightarrow \mathrm{F}_{\mathrm{T}}=\frac{200}{3}=66.66$
Force on each mount $=\frac{66.66}{2}=33.33$
38. A bar is compressed to half of its original length. The magnitude of true strain produced in the deformed bar is $\qquad$ (correct to two decimal places).

Key: (0.693)
Sol: $\quad \varepsilon=\ln \left(\frac{\ell_{\mathrm{f}}}{\ell_{\mathrm{i}}}\right) \Rightarrow \varepsilon=\ln 0.5$
$\varepsilon=-0.693$
But magnitude of true strain $=0.693$
39. A carpenter glues a pair of cylindrical wooden logs by bonding their end faces at an angle of $\theta=$ $30^{\circ}$ as shown in the figure.


The glue used at the interface fails if
Criterion 1: the maximum normal stress exceeds 2.5 MPa .
Criterion 2: the maximum normal stress exceeds 1.5 MPa .
Assume that the interface fails before the logs fail. When a uniform tensile stress of 4 MPa is applied, the interface
(A) fails only because of criterion 1
(B) fails only because of criterion 2
(C) fails because of both criterion 1 and 2
(D) does not fail

Key: (C)
Sol: $\quad \theta=30^{\circ} \Rightarrow \sigma=\frac{\mathrm{P}}{\mathrm{A}}=4 \mathrm{MPa}$

$$
\begin{aligned}
\sigma_{\theta} & =\frac{\mathrm{P}}{\mathrm{~A}} \cos ^{2} \theta \\
& =4 \cos ^{2} 30=3 \mathrm{MPa}>2.5 \mathrm{MPa} \\
\tau_{\theta} & =\frac{\mathrm{P}}{2 \mathrm{~A}} \sin 2 \theta \Rightarrow \tau_{\theta}=\frac{4}{2} \sin 60^{\circ}=1.732>1.5 \mathrm{MPa}
\end{aligned}
$$

## Fails by both Criterion 1 and 2

40. In a Lagrangian system, the position of a fluid particle in a flow is described as $x=x_{0} e^{-k t}$ and $Y=y_{0} e^{k t}$ where t is the time while $x_{0}, y_{0}$, and k are constants. The flow is
(A) unsteady and one-dimensional
(B) steady and two-dimensional
(C) steady and one-dimensional
(D) unsteady and two-dimensional

## Key: (B)

Sol: $\quad \because \mathrm{u}=\frac{\mathrm{dx}}{\mathrm{dt}}$
$\mathrm{u}=-\mathrm{kx}_{\mathrm{o}} \mathrm{e}^{-\mathrm{kt}} \Rightarrow \mathrm{u}=-\mathrm{kx}$
$\& v=\frac{d y}{d t} \Rightarrow v=k y$

So, $\overrightarrow{\mathrm{V}}=-\mathrm{kxi}+\mathrm{kyj}$
i.e, $\vec{V} \neq f(t)$

So, steady flow \& $\vec{V}=f(x, y)$. So, 2D flow.
41. Processing times (including setup times) and due dates for six jobs waiting to be processed at a work centre are given in the table. The average tardiness (in days) using shortest processing time rule is $\qquad$ (correct to two decimal places).

| Job | Processing time (days) | Due date (days) |
| :---: | :---: | :---: |
| $A$ | 3 | 8 |
| $B$ | 7 | 16 |
| C | 4 | 4 |
| $D$ | 9 | 18 |
| $E$ | 5 | 17 |
| $F$ | 13 | 19 |

Key: (6.33)
Sol: By SPT rule

| Job Sequence | P.T | Machining |  | D.D | Tardiness |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | In | Out |  |  |
| A | 3 | 0 | 3 | 8 | 0 |
| C | 4 | 3 | 7 | 4 | 3 |
| E | 5 | 7 | 12 | 17 | 0 |
| B | 7 | 12 | 19 | 16 | 3 |
| D | 9 | 19 | 28 | 18 | 10 |
| F | 13 | 28 | 41 | 19 | 22 |

Total Tardiness $=38$
Average Tardiness $=\frac{38}{6}=6.33$ days
42. Steam flows through a nozzle at mass flow rate of $\dot{\mathrm{m}}=0.1 \mathrm{~kg} / \mathrm{s}$ with a heat loss of 5 kW . The enthalpies at inlet and exit are $2500 \mathrm{~kJ} / \mathrm{kg}$ and $2350 \mathrm{~kJ} / \mathrm{kg}$, respectively. Assuming negligible velocity at inlet $\left(\mathrm{C}_{1} \approx 0\right)$, the velocity $\left(\mathrm{C}_{2}\right)$ of steam (in $\left.\mathrm{m} / \mathrm{s}\right)$ at the nozzle exit is $\qquad$ (correct to two decimal places)


Key: (447.21)
Sol: $\quad \dot{\mathrm{m}}=0.1 \mathrm{~kg} / \mathrm{sec}, \mathrm{Q}=-5 \mathrm{~kW}$ (Heat Rejected)
$\mathrm{h}_{1}=2500 \mathrm{~kJ} / \mathrm{kg}, \mathrm{h}_{2}=2350 \mathrm{~kJ} / \mathrm{kg}$


Applying steady flow energy equation
$\dot{\mathrm{m}}\left(\mathrm{h}_{1}+\frac{\mathrm{C}_{1}^{2}}{2000}\right)+\dot{\mathrm{Q}}=\dot{\mathrm{m}}\left(\mathrm{h}_{2}+\frac{\mathrm{C}_{2}^{2}}{2000}\right)+\mathrm{W}$
$\mathrm{W}=0$, since no work done, $\mathrm{C}_{1}=0$
$\Rightarrow 0.1(2500)-5=0.1\left(2350+\frac{\mathrm{C}_{2}^{2}}{2000}\right)$
$245=0.1\left(2350+\frac{\mathrm{C}_{2}^{2}}{2000}\right) \Rightarrow 2450=2350+\frac{\mathrm{C}_{2}^{2}}{2000}$
$\Rightarrow \mathrm{C}_{2}=447.21 \mathrm{~m} / \mathrm{sec}$
43. A point mass is shot vertically up from ground level with a velocity of $4 \mathrm{~m} / \mathrm{s}$ at time, $t=0$. It loses $20 \%$ of its impact velocity after each collision with the ground. Assuming that the acceleration due to gravity is $10 \mathrm{~m} / \mathrm{s}^{2}$ and that air resistance is negligible, the mass stops bouncing and comes to complete rest on the ground after a total time (in seconds) of
(A) 1
(B) 2
(C) 4
(D) $\infty$

Key: (C)
Sol: $\quad \mathrm{V}_{1}=4 \mathrm{~m} / \mathrm{sec}, \mathrm{V}_{2}=0.8 \times 4=3.2 \mathrm{~m} / \mathrm{sec}$

$$
\begin{aligned}
& \mathrm{V}_{1}=\mathrm{V} \Rightarrow \mathrm{t}_{1}=\frac{2 \mathrm{~V}_{1}}{\mathrm{~g}} \\
& \mathrm{~V}_{2}=0.8 \mathrm{~V} \Rightarrow \mathrm{t}_{2}=\frac{2 \mathrm{~V}_{2}}{\mathrm{~g}} \\
& \mathrm{~V}_{3}=0.64 \mathrm{~V} \Rightarrow \mathrm{t}_{3}=\frac{2 \mathrm{~V}_{3}}{\mathrm{~g}} \\
& \mathrm{~T}=\mathrm{t}_{1}+\mathrm{t}_{2}+\ldots . . . . . . . . . . . \\
& =\left[\frac{2 \mathrm{~V}_{1}}{\mathrm{~g}}+\frac{2 \mathrm{~V}_{2}}{\mathrm{~g}}+\frac{2 \mathrm{~V}_{3}}{\mathrm{~g}}+\ldots \ldots . .\right] \\
& =\frac{2}{10} \times 4[1+0.8+0.64+\ldots . .] \\
& =\frac{2}{10} \times 4\left[1+0.8+(0.8)^{2}+\ldots . . \infty\right] \\
& =0.8 \times \frac{1}{1-0.8}=\frac{0.8}{0.2}=4=4 \mathrm{sec}
\end{aligned}
$$

44. A tank of volume $0.05 \mathrm{~m}^{3}$ contains a mixture of saturated water and saturated steam at $200^{\circ} \mathrm{C}$. The mass of the liquid present is 8 kg . The entropy (in $\mathrm{kJ} / \mathrm{kgK}$ ) of the mixture is $\qquad$ (correct to two decimal places)

Property data for saturated steam and water are:
At $200^{\circ} \mathrm{c}, \mathrm{P}_{\text {sat }}=1.5538 \mathrm{MPa}$
$v_{\mathrm{f}}=0.001157 \mathrm{~m}^{3} / \mathrm{kg}, v_{g}=0.12736 \mathrm{~m}^{3} / \mathrm{kg}$
$s_{f g}=4.1014 \mathrm{~kJ} / \mathrm{kgK}, s_{\mathrm{f}}=2.3309 \mathrm{~kJ} / \mathrm{kgK}$
Key: (2.49)
Sol: $\quad V=0.05 \mathrm{~m}^{3}, \mathrm{~T}_{\text {sat }}=200^{\circ} \mathrm{C}, \mathrm{m}_{\mathrm{L}}=8 \mathrm{~kg}$
At $200^{\circ} \mathrm{C}, \mathrm{P}_{\text {sat }}=1.5538 \mathrm{MPa}$
$\mathrm{v}_{\mathrm{f}}=0.001157 \mathrm{~m}^{3} / \mathrm{kg}, \mathrm{v}_{\mathrm{g}}=0.12736 \mathrm{~m}^{3} / \mathrm{kg}$
$\mathrm{s}_{\mathrm{fg}}=4.1014 \mathrm{~kJ} / \mathrm{kgK}, \mathrm{s}_{\mathrm{f}}=2.3309 \mathrm{~kJ} / \mathrm{kgK}$

Given container has both water vapor \& liquid
i.e., it is in wet-vapour region,

In that case entropy of mixture is $\mathrm{s}=\mathrm{s}_{\mathrm{f}}+\mathrm{Xs}_{\mathrm{fg}}$

Where $x=$ dryness fraction $=\frac{m_{v}}{m_{v}+m_{L}}$
$\mathrm{v}_{\mathrm{f}(\text { liquid })}=\mathrm{m}_{\mathrm{L}} \mathrm{v}_{\mathrm{f}}=(8)(0.001157)$
$\mathrm{v}_{\mathrm{f}(\text { liquid })}=0.01$
$\mathrm{v}_{\text {vapour }}=\mathrm{v}-\mathrm{v}_{\mathrm{f} \text { (liquid) }}=0.05-0.01=0.04 \mathrm{~m}^{3}$
$\mathrm{m}_{\mathrm{v}}=\frac{\mathrm{v}_{\text {vapour }}}{\mathrm{v}_{\mathrm{g}}}=\frac{0.04}{0.12736}=0.31 \mathrm{~kg}$
$x=\frac{0.31}{(0.31+8)}=0.04$
$\therefore \mathrm{s}=2.3309+0.04(4.1014)=2.49 \mathrm{~kJ} / \mathrm{kgK}$
45. A tank open at the top with a water level of 1 m , as shown in the figure, has a hole at a height of 0.5 m . A free jet leaves horizontally from the smooth hole. The distance $X$ (in m ) where the jet strikes the floor is

(A) 0.5
(B) 1.0
(C) 2.0
(D) 4.0

Key: (B)
Sol: $u_{x}=\sqrt{2 \times 9.81 \times 0.5}=3.13$
$u_{y}=0$
$\because s_{y}=u_{y} t+\frac{1}{2} a_{y} t^{2} \Rightarrow t=\sqrt{\frac{1}{g}}$
$\mathrm{s}_{\mathrm{x}}=\mathrm{u}_{\mathrm{x}}+\frac{1}{2} \mathrm{a}_{\mathrm{x}} \mathrm{t}^{2} \Rightarrow \mathrm{~s}_{\mathrm{x}}=3.13 \times \sqrt{\frac{1}{\mathrm{~g}}}$
(here $\mathrm{a}_{\mathrm{x}}=0$ )
$\mathrm{s}_{\mathrm{x}}=1 \mathrm{~m}$
46. A self-aligning ball bearing has a basic dynamic load rating ( $\mathrm{C}_{10}$, for $10^{6}$ revolutions) of 35 kN . If the equivalent radial load on the bearing is 45 kN , the expected life (in $10^{6}$ revolutions) is
(A) below 0.5
(B) 0.5 to 0.8
(C) 0.8 to 1.0
(D) above 1.0

Key: (A)
Sol: $\quad P_{e}=45 k N ; C=35 k N$
$\mathrm{L}_{10}=\left(\frac{\mathrm{C}}{\mathrm{P}_{\mathrm{e}}}\right)^{3}=\left(\frac{35}{45}\right)^{3}=0.47<0.5$
47. A simply supported beam of width 100 mm , height 200 mm and length 4 m is carrying a uniformly distributed load of intensity $10 \mathrm{kN} / \mathrm{m}$. The maximum bending stress (in MPa) in the beam is $\qquad$ (correct to one decimal place)


Key: (30)
Sol: $\quad \sigma=\frac{M}{I} y, M=\frac{w L^{2}}{8}=\frac{10 \times 4^{2}}{8}=20 \mathrm{kN}-\mathrm{m}$
$\mathrm{I}=\frac{100 \times 200^{3}}{12}=66.67 \times 10^{6}$
$y=\frac{200}{2}=100$;
$\sigma=\frac{20 \times 10^{6}}{66.67 \times 10^{6}} \times\left(\frac{200}{2}\right)=30 \mathrm{MPa}$
48. The schematic of an external drum rotating clockwise engaging with a short shoe is shown in the figure. The shoe is mounted at point Y on a rigid lever XYZ hinged at point X . A force $\mathrm{F}=100 \mathrm{~N}$ is applied at the free end of the lever as shown. Given that the coefficient of friction between the shoe and the drum is 0.3 , the braking torque (in Nm) applied on the drum is $\qquad$ (correct to two decimal places).
Key: (8.18)
Sol: $\quad \Sigma \mathrm{M}_{\mathrm{x}}=0$

(All dimensions are in mm )
$\left(\mathrm{R}_{\mathrm{N}} \times 200\right)-\left(\mu \mathrm{R}_{\mathrm{N}} \times 300\right)-(\mathrm{F} \times 300)=0$
$\left(\mathrm{R}_{\mathrm{N}} \times 200\right)-\left(0.3 \times \mathrm{R}_{\mathrm{N}} \times 300\right)-(100 \times 300)=0$
$\mathrm{R}_{\mathrm{N}}=\frac{(100 \times 300)}{(200-(0.3 \times 300))}=272.72 \mathrm{~N}$
$\mathrm{T}=\mu \mathrm{R}_{\mathrm{N}} \times$ Radius $=8.18 \mathrm{~N}-\mathrm{mts}$
49. The state of stress at a point, for a body in plane stress, is shown in the figure below. If the minimum principal stress is 10 kPa , then the normal stress $\sigma_{\mathrm{y}}($ in kPa$)$ is

(A) 9.45
(B) 18.88
(C) 37.78
(D) 75.50

Key: (C)
Sol: $\quad \sigma_{2}=\left[\frac{\sigma_{x}+\sigma_{y}}{2}\right]-\sqrt{\left(\frac{\sigma_{x}-\sigma_{y}}{2}\right)^{2}+T_{x y}^{2}}$
$10=\left[\frac{100+\sigma_{y}}{2}\right]-\sqrt{\left(\frac{100-\sigma_{y}}{2}\right)^{2}+50^{2}}$
$\left[10-\left[\frac{100+\sigma_{y}}{2}\right]\right]^{2}=\left(\frac{100-\sigma_{y}}{2}\right)^{2}+50^{2}$
$100-2 \times 10 \times\left(\frac{100+\sigma_{y}}{2}\right)=\left(\frac{100-\sigma_{y}}{2}\right)^{2}-\left(\frac{100+\sigma_{y}}{2}\right)^{2}+2500$
$100-1000-10 \sigma_{y}=\frac{-4 \times 100 \times \sigma_{y}}{4}+2500$
$90 \sigma_{y}=2500+1000-100 \Rightarrow \sigma_{y}=37.77 \mathrm{MPa}$
50. An electrochemical machining (ECM) is to be used to cut a through hole into a 12 mm thick aluminium plate. The hole has a rectangular cross-section, $10 \mathrm{~mm} \times 30 \mathrm{~mm}$. The ECM operation will be accomplished in 2 minutes, with efficiency of $90 \%$. Assuming specific removal rate for aluminium as $3.44 \times 10^{-2} \mathrm{~mm}^{3} /(\mathrm{A} \mathrm{s})$, the current (in A) required is $\qquad$ (correct to two decimal places).

Key: (968.99)
Sol: Volume to be removed $=10 \times 30 \times 12=3600 \mathrm{~mm}^{3}$
Energy required $==\frac{3600}{3.44 \times 10^{-2} \times 0.9}=116279 \mathrm{As}$
Current $=\frac{116279}{120}=968.99 \mathrm{~A}$
51. An engine working on air standard Otto cycle is supplied with air at 0.1 MPa and $35^{\circ} \mathrm{C}$. The compression ratio is 8 . The heat supplied is $500 \mathrm{~kJ} / \mathrm{kg}$. Property data for air: $\mathrm{c}_{\mathrm{p}}=1.005 \mathrm{~kJ} / \mathrm{kgK}, \mathrm{c}_{\mathrm{v}}=$ $0.718 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}, \mathrm{R}=0.287 \mathrm{~kJ} / \mathrm{kg} \mathrm{K}$. The maximum temperature (in K ) of the cycle is $\qquad$ (correct to one decimal place).
Key: (1403.98)
Sol: $\quad \mathrm{P}=0.1 \mathrm{MPa}, \mathrm{T}_{1}=35^{\circ} \mathrm{C}, \mathrm{r}_{\mathrm{c}}=8$
$\mathrm{Q}_{\text {supplied }}=500 \mathrm{~kJ} / \mathrm{kg}$
$\mathrm{C}_{\mathrm{p}}=1.005 \mathrm{~kJ} / \mathrm{kgK}$,
$\mathrm{C}_{\mathrm{V}}=0.718 \mathrm{~kJ} / \mathrm{kgK}$,
$\mathrm{R}=0.287 \mathrm{~kJ} / \mathrm{kgK}$
$\mathrm{T}_{1}=35+273=308 \mathrm{~K}$

$\frac{\mathrm{T}_{2}}{\mathrm{~T}_{1}}=\left(\frac{\mathrm{V}_{1}}{\mathrm{~V}_{2}}\right)^{\gamma-1}=\mathrm{r}_{\mathrm{c}}^{\gamma-1}$
$\Rightarrow \mathrm{T}_{2}=(308)(8)^{(1.4-1)}=707.60 \mathrm{~K}$
$\mathrm{Q}_{\text {supplied }}=\mathrm{C}_{\mathrm{v}}\left(\mathrm{T}_{3}-\mathrm{T}_{2}\right)$
$500=(0.718)\left(\mathrm{T}_{3}-707.60\right)$
$\mathrm{T}_{3}=1403.98 \mathrm{~K}$
52. An orthogonal cutting operation is being carried out in which uncut thickness is 0.010 mm , cutting speed is $130 \mathrm{~m} / \mathrm{min}$, rake angle is $15^{\circ}$ and width of cut is 6 mm . It is observed that the chip thickness is 0.015 mm , the cutting force is 60 N and the thrust force is 25 N . The ratio of friction energy to total energy is $\qquad$ (correct to two decimal places).
Key: (0.4406)
Sol: $\mathrm{t}_{1}=0.01 \mathrm{~mm} ; \mathrm{v}=130 \mathrm{~m} / \mathrm{min} ; \alpha=15^{\circ}$
$\mathrm{b}=6 \mathrm{~mm} ; \mathrm{t}_{\mathrm{c}}=0.015 \mathrm{~mm}$,
cutting force $=\mathrm{F}_{\mathrm{H}}=60 \mathrm{~N}$
Thrust force $=\mathrm{F}_{\mathrm{v}}=25 \mathrm{~N}$

[^1]$\mathrm{R}=\sqrt{60^{2}+25^{2}}=65 \mathrm{~N}$
$\mathrm{F}=\mathrm{R} \sin \lambda=39.66 \mathrm{~N}$
$\tan (\lambda-\alpha)=\frac{\mathrm{F}_{\mathrm{v}}}{\mathrm{F}_{\mathrm{H}}}=\frac{25}{60}=22.61$
$\lambda=37.61$
$\frac{\text { Friction energy }}{\text { Total energy }}=\frac{F}{F_{H}} \cdot \frac{t_{1}}{t_{c}}=0.4406$

53. An explicit forward Euler method is used to numerically integrate the differential equation
$$
\frac{\mathrm{dy}}{\mathrm{dt}}=\mathrm{y}
$$
using a time step of 0.1 . With the initial condition $\mathrm{y}(0)=1$, t he value of $\mathrm{y}(1)$ computed by this method is $\qquad$ (correct to two decimal places).

Key: (2.59)
Sol: By Euler method,
$\mathrm{y}_{\mathrm{n}+1}=\mathrm{y}_{\mathrm{n}}+\mathrm{nf}\left(\mathrm{t}_{\mathrm{n}}, \mathrm{y}_{\mathrm{n}}\right)$
where given $\mathrm{f}(\mathrm{t}, \mathrm{y})=\mathrm{y}$
$\therefore y_{n+1}=y_{n}+h y_{n}$
$\Rightarrow y_{n+1}=(1+h) y_{n}$
$y_{1}=y(0.1)=(1+0.1) \times 1=1.1 \quad\left(\because y_{0}=1\right)$
$y_{2}=y(0.2)=1.1 \times 1.1$
$y_{3}=y(0.3)=1.1 \times(1.1 \times 1.1)$
$y_{10}=y(1)=(1.1)^{10} \simeq 2.59$
54. The maximum reduction in cross-sectional area per pass $(\mathrm{R})$ of a cold wire drawing process is

$$
\mathrm{R}=1-\mathrm{e}^{-(\mathrm{n}+1)}
$$

where n represents the strain hardening coefficient. For the case of a perfectly plastic material, $R$ is
(A) 0.865
(B) 0.826
(C) 0.777
(D) 0.632

Key: (D)
Sol: $\because$ for perfectly plastic material, $\mathrm{n}=0$
So, $R=1-e^{-1} \Rightarrow R=0.632$
55. A sprinkler shown in the figure rotates about its hinge point in a horizontal plane due to water flow discharged through its two exit nozzles.


The total flow rate Q through the sprinkler is 1 litre/sec and the cross-sectional area of each exit nozzle is $1 \mathrm{~cm}^{2}$. Assuming equal flow rate through both arms and a frictionless hinge, the steady state angular speed of rotation ( $\mathrm{rad} / \mathrm{s}$ ) of the sprinkler is $\qquad$ (correct to two decimal places).

Key: (10)
Sol: $\quad u_{1}=u_{2}=\frac{\mathrm{Q}}{2 \mathrm{~A}}=\frac{1 \times 10^{-3}}{2 \times 10^{-4}}=5 \mathrm{~m} / \mathrm{s}$
Now Absolute velocity
$\mathrm{v}_{1}=\mathrm{u}_{1}+\mathrm{r}_{1} \omega$
$\mathrm{v}_{2}=\mathrm{u}_{2}-\mathrm{r}_{2} \omega$
$\because$ external Torque $=0$

$\cdot \cos ^{2}$
$\omega$
$\dot{\mathrm{m}}_{1} \mathrm{v}_{1} \mathrm{r}_{1}-\dot{\mathrm{m}}_{2} \mathrm{v}_{2} \mathrm{r}_{2}=0 \quad\left(\because \dot{\mathrm{~m}}_{1}=\dot{\mathrm{m}}_{2}\right)$
$\Rightarrow \omega=10 \mathrm{rad} / \mathrm{s}$

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Agartala 9856034530 |Agra 9760012902 | Ahmedabad $8401699466 \mid$ Ajmer 9829075765 | Aligarh $9761636422 \mid$ Allahabad $9839330710 \mid$ Amravati 8237551611 | Bangalore 9886600010 | Bilaspur 9993973456 | Calicut 9961969988 | Chandigarh 9317607007 | Chennai 9677030010 |Coimbatore 8883332556 | Delhi (Pitampura) 9718612147 | Delhi (Saket) 8587010876 | Ghaziabad 9910101602 |Gorakhpur 8574598018 |Greater Noida 9891990434 Hyderabad (Abids) 9989477436 | Hyderabad (Dilsukhnagar) 9581626677 | Indore 9826010276 | Jaipur 8290089245 | Jalandhar 7696197007 | Kanchipuram 8695554546 | Kanpur 9839234875 | Kochi 8113020304 | Kolhapur 9763631729 | Kolkata (Minto Park) 9007889898 | Kolkata (Vip Road) 9831891898 | Kollam 9048497233 | Madurai 8754029058 | Mumbai (Dadar) 9967897127 | Mumbai (Thane) 7893336874 | Mysore 9980155550 | Nagpur 7767001955 Nanded 9172263930 | Nashik 8888559922 | Noida 9560983851 | Pune 9561133868 | Rajkot 9909986464 | Ranchi 8804445566 | Silchar $9957577496 \mid$ Surat 9377859870 | Srinagar 9906475295 Trichy 7667369058 | Trivandrum 9447132291 | V V Nagar 7778829064 | Vadodara 8401646906
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