Electromagnetic Theory

- Dot product (scalar), $\vec{A} \cdot \vec{B} = |A| |B| \cos \theta_{AB}$
- Vector product $\overrightarrow{A} \times \overrightarrow{B} = |A||B|\sin\theta_{AB} \cdot \overrightarrow{n}$
- Scalar triple product

$$\overrightarrow{A} \cdot (\overrightarrow{B} \times \overrightarrow{C}) = \overrightarrow{B} \cdot (\overrightarrow{C} \times \overrightarrow{A}) = \overrightarrow{C} (\overrightarrow{A} \times \overrightarrow{B})$$

Vector triple product

$$\overrightarrow{\mathbf{A}} \times \left(\overrightarrow{\mathbf{B}} \times \overrightarrow{\mathbf{C}} \right) = \overrightarrow{\mathbf{B}} \left(\overrightarrow{\mathbf{A}} \cdot \overrightarrow{\mathbf{C}} \right) - \overrightarrow{\mathbf{C}} \left(\overrightarrow{\mathbf{A}} \cdot \overrightarrow{\mathbf{B}} \right)$$

- Value of gradient:
 - (a) In Cartesian coordinates

$$\nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z$$

(b) In cylindrical coordinate

$$\nabla V = \frac{\partial V}{\partial \rho} \hat{\mathbf{a}}_{\rho} + \frac{1}{\rho} \frac{\partial V}{\partial \phi} \hat{\mathbf{a}}_{\phi} + \frac{\partial V}{\partial z} \hat{\mathbf{a}}_{z}$$

(c) In spherical polar coordinates

$$\nabla \mathbf{V} = \frac{\partial \mathbf{V}}{\partial \mathbf{r}} \hat{\mathbf{a}}_{\mathbf{r}} + \frac{1}{\mathbf{r}} \frac{\partial \mathbf{V}}{\partial \boldsymbol{\theta}} \hat{\mathbf{a}}_{\boldsymbol{\theta}} + \frac{1}{\mathbf{r} \sin \boldsymbol{\theta}} \frac{\partial \mathbf{V}}{\partial \boldsymbol{\phi}} \hat{\mathbf{a}}_{\boldsymbol{\phi}}$$

- Values of Divergence
 - (a) In Cartesian coordinates

$$\nabla \cdot \overrightarrow{\mathbf{A}} = \frac{\partial \mathbf{A}_{\mathbf{x}}}{\partial \mathbf{x}} + \frac{\partial \mathbf{A}_{\mathbf{y}}}{\partial \mathbf{y}} + \frac{\partial \mathbf{A}_{\mathbf{z}}}{\partial \mathbf{z}}$$

(b) In Cylindrical coordinate

$$\nabla \cdot \overline{A} = \frac{1}{\rho} \frac{\partial \left(\rho A_{\rho} \right)}{\partial \rho} + \frac{1}{\rho} \frac{\partial A_{\phi}}{\partial \phi} + \frac{\partial A_{z}}{\partial z}$$

(c) In Spherical polar coordinate

$$\nabla \cdot \overrightarrow{A} = \frac{1}{r^2} \frac{\partial (r^2 A_r)}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial (\sin \theta A_\theta)}{\partial \theta} + \frac{1}{r \sin \theta}$$

- Divergence theorem $\int_{V} \nabla \cdot \overrightarrow{A} dv = \oint_{S} \overrightarrow{A} \cdot d\overrightarrow{s}$
- Stoke's theorem $\oint_{L} \vec{A} \cdot d\vec{l} = \int_{S} \nabla \times \vec{A} \cdot d\vec{s}$

Gauss's Law-
$$\vec{D} = \varepsilon \vec{E} = \frac{Q}{4\pi r^2} \hat{a}_r$$

Flux density $\overline{\mathbf{D}} = \varepsilon \overline{\mathbf{E}}$

Electric flux as $\psi = \overline{D} .ds$

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Poisson's equation
$$\nabla^2 V = -$$

Poisson's equation $\nabla^2 V = -\frac{\rho_V}{\epsilon}$ Laplace's equation $\nabla^2 V = 0$

Magnetic Force $F = \int (I \times B) d\ell = BIL$ Biot-Savartlaw $d\vec{H} = \frac{Id\vec{l} \times \hat{a}_R}{4\pi R^2} = \frac{Id\vec{l} \times \vec{R}}{4\pi R^3}$

Ampere's Circuital Law

 $\Phi \vec{H} \cdot d\vec{l} = \vec{I}_{enc} \text{ OR } \nabla \times \vec{H} = \vec{J}$

Boundary Conditions (FOR ELECTRIC FIELD): Tangential component

 $D_{1n} - D_{2n} = \rho_s$

 $\varepsilon_1 \mathbf{E}_{1n} - \varepsilon_2 \mathbf{E}_{2n} = \rho_s$

Tangential component
$$E_{1t} = E_{2t} \text{ or } \frac{D_{1t}}{\varepsilon_1} = \frac{D_{2t}}{\varepsilon_2}$$
Normal component

For normal component For tangential component $B_{1n} = B_{2n} H_{1t} - H_{2t} = J_{Sn}$

magnetic fiels):

Boundary Conditions(FOR

Energy stored in Magnetic Field $W = \int_0^I Lidi = \frac{1}{2}LI^2 Joule$

- Poynting Vector $\vec{P} = \vec{E} \times \vec{H}$
- Value of attenuation, phase constant for per fect dielectric are $\alpha = \frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}}$, $\beta = \omega \sqrt{\mu \epsilon}$.
- Skin Depth $\partial = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega u \sigma}}$
- Reflection coefficient $\tau = \frac{\eta_2 \eta_1}{\eta_2 + \eta_1}$ and transission coefficient $T = \frac{2\eta_2}{\eta_1 + \eta_2} = 1 + \tau$
- Standing wave ratio $S = \frac{|E|_{\text{max}}}{|E|_{\text{min}}} = \frac{1 + |\Gamma|}{1 |\Gamma|}$ Brewster angle $\tan \theta_B = \sqrt{\frac{\epsilon_2}{\epsilon_1}}$

line
$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Impedance at any Point on the Line

$$Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta \ell}{Z_0 + jZ_L \tan \beta \ell} \right]$$

- Return loss (RL) = $-20 \log |\Gamma_L| dB$
- Approximate beam width of horn antenna

$$\theta_{\rm E} = \frac{56 \, \lambda^{\rm o}}{\rm h}$$
 and $\theta_{\rm H} = \frac{67 \, \lambda^{\rm o}}{\rm w}$

Directivity of horn $D = \frac{7.5 \text{ A}}{1.5 \text{ A}}$

$$D = \frac{7.5 \text{ A}}{\lambda^2}$$

Maximum Radar Range (R____

$$R_{max} = \left[\frac{P_t \cdot G \sigma A_e}{(4\pi)^2 \cdot S_{min}} \right]^{\frac{1}{4}}$$

Maximum unambiguous range

$$R_{unamb} = \frac{c(T_{ON} + T_{FF})}{2} = \frac{c}{2 prf}$$